

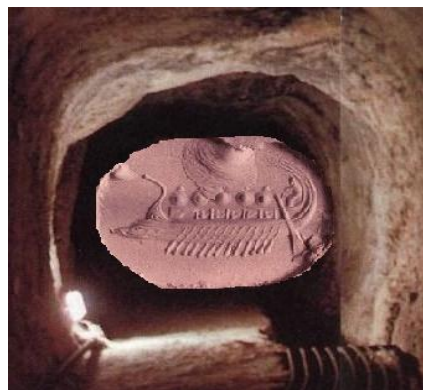
**ΕΘΝΙΚΟ ΜΕΤΣΟΒΙΟ ΠΟΛΥΤΕΧΝΕΙΟ**  
**ΣΧΟΛΗ ΝΑΥΠΗΓΩΝ ΜΗΧΑΝΟΛΟΓΩΝ ΜΗΧΑΝΙΚΩΝ**  
**ΔΠΜΣ: "ΝΑΥΤΙΚΗ ΚΑΙ ΘΑΛΑΣΣΙΑ ΤΕΧΝΟΛΟΓΙΑ ΚΑΙ ΕΠΙΣΤΗΜΗ"**

**ΜΕΤΑΠΤΥΧΙΑΚΗ ΔΙΠΛΩΜΑΤΙΚΗ ΕΡΓΑΣΙΑ**

ΘΕΜΑ: "ΔΥΝΑΜΙΚΗ ΑΛΛΗΛΕΠΙΔΡΑΣΗ ΛΕΠΤΟΓΡΑΜΜΩΝ ΘΑΛΑΣΣΙΩΝ  
ΑΓΩΓΩΝ ΜΕ ΤΟΝ ΠΥΘΜΕΝΑ"

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Επιβλ. καθηγητής: Ιωάννης Χατζηγεωργίου



ΑΘΗΝΑ, ΙΟΥΛΙΟΣ 2011

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( , ,2 . . . )

# EXOMENA

		7
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/

- Riser (Steel Catenary Riser)

, , ,

riser ( . . . )

riser, )

, ' ,

,

"sagbend" ( riser -Touch Down  
Point/TDP- )

" "

riser,

.

/ riser ,

,

,

, Phase2.

- ,

TDP,

,

riser,

TDP,



Phase 2, Rocscience, : "Three dimensional nonlinear dynamics of submerged, extensible catenary pipes conveying fluid and subjected to end-imposed excitations" [7].

Phase2, Rocscience,

## ABSTRACT

In the present thesis, an effort has been made for quantification of the effect of soil reaction in the motion of a slender Steel Catenary Riser structure -used for the transport of hydrocarbons from offshore fields- and, sequentially, import of the defined values of soil reaction forces to a published nonlinear dynamic model of Finite Differences that identifies the dominating dynamic parameters of the induced motion of the Riser due to harmonic excitations applied on the top end of the structure (e.g. harmonic wave-induced movements of the floating platform which binds the riser, etc). Based on observations of the contemporary international research, such harmonic moves are, by definition, the major sources of fatigue damage, especially at the most vulnerable area "sagbend" (the area of the riser before the Touch Down Point / TDP - up to it) exhibiting the maximum curvature, and are the fundamental causes for trench formations created at the surface of the bottom due to consequent movements of the lower section of the riser, the bottom laying part.

The determination of the soil reaction is static, assuming that the riser has completed the cycle of embedment in the soil, for various penetration depths and various excavation geometries, as well, based on previously published experimental observations. At first, the plain stress condition of the soil, for all cases of penetration depths and trench formations, is accomplished with the contribution of the Geotechnical, commercial software, Phase2. Then the stresses are integrated around the arched riser-soil contact surface for the production of vertical soil-reacting forces in the penetration of the riser, for each case of the examined trench formations, as well. Finally, these force-values are imported as concentrated loads applied at the TDP, in the existing nonlinear dynamic model, which is then solved for various cases of harmonic excitations applied on top of the riser, in order to test the effect of TDP soil reaction in the various dynamic parameters involved in fatigue damage.

The non-linear dynamic model has been published on the work of Assoc. Prof. I. Chatjigeorgiou: "*Three dimensional nonlinear dynamics of submerged, extensible catenary pipes conveying fluid and subjected to end-imposed excitations*" [7]. The Geotechnical Code, Phase2, by Rocscience, is a property of the Laboratory of Structural Engineering and Elements of Structures, School of Rural and Surveying Engineering, NTUA, chaired by Professor Michael Sakellariou, who provided it for all necessary calculations.



1.

, Steel Catenary Risers (SCR).

SCR.

1500

3.000

SCR

SCR

- SCR system,

riser

TDP (Touch Down Point).

« »

[12, 15, 46].

riser

(Phase 2).

z, [7], (in-plane, x ó).

**1.1**

**SCR.**

ó [10]. ( . . : *drill-ship*)

SCR  
[10].

(buckling)

(FEM),

( )

## 1.2

**riseró** .

20 ,

riser-

õ

ö

:

Bridge et al. [33], 2001 2003,

õ

ö

riser-

:

- H õ ö ( ó ),  
, ( )  
)

ó

•

« »

•

(scour)

•

"Vortex Induced Vibrations"

«

»

•

(*lift force* + )

Aubeny et al. [2, 4]

riser

( ),

( k)

ó

[1, 3],

Euler - Bernoulli  
Winkler"

(

American Society of Civil Engineers

(ASCE 2005)

õ

ö,

õ

ö

, *strip foot foundations* [51]

"

"

Dendani, France and Jaeck [48], 2008

Norwegian Geotechnical Institute (2005),

riser

Hansen [46] Terzaghi (1943)

Hansen,

Verley and Lund

[47].

risers

risers

Verley and Lund [47], 1995.

risers

S-Lay

J-Lay

Hansen:

$$\frac{z_{init}}{D} = 0.0071(S * G^{0.3})^{3.2} + 0.062(S * G^{0.3})^{0.7}$$

D

, S

G

Su

Verley Lund

2000-2010 [54].

Nakhaee and Zhang [5],

P-y (

/

-

/

)

riser

/

riser

riser.

riser

riser -

, TDZ (Touch Down Zone).





2.

-

2.1

riseró

, , -

, .

TDP ( riser ), riser

,

.

riser ( ) ( / )

,

).

riser, , riser " "

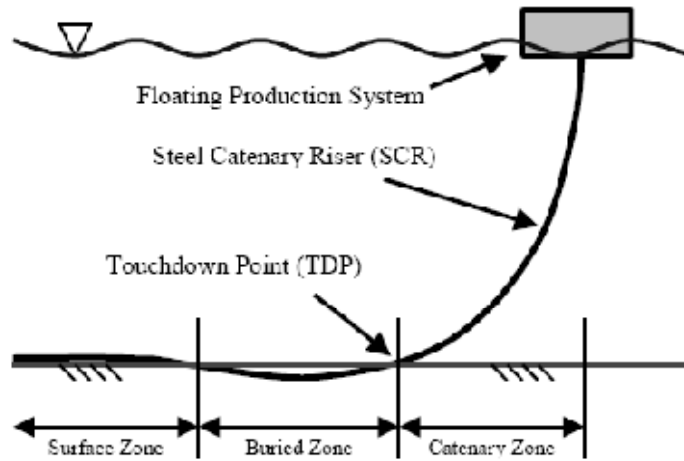
.

,

.

riser, (scour)

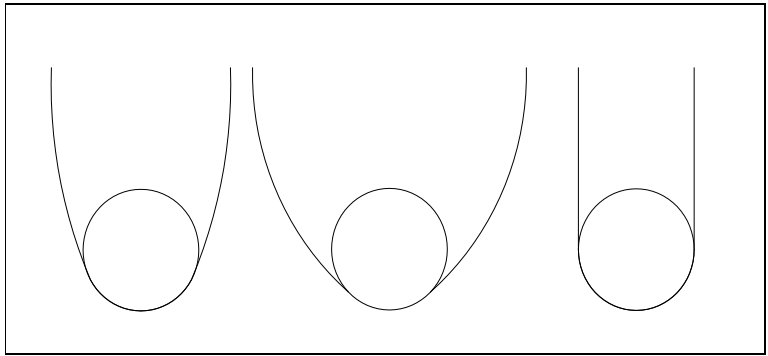
[9, 33]



2.1: riser ( : Bridge et al., 2003)

- riser TDP, : riser „
- riser ( 2.1) [33]. riser 2 , TDP. buried zone surface-zone.
- ( )

- motions) riser, (surge) (heave), riser, riser,  $\delta U \ddot{u}$  (2.2).



2.2:

riser

[10].

" " ( , , , . .)

2.2

riser

( 2.2.).

riser

. 2.1

$$F_{sr} = R \int \sigma \sin \theta d\theta$$

Fsr

, Phase 2

(Rocscience Ltd.).

riser

"CON3DF" [7]

Fortran.

x, y

/ z

/

TDP,  
( kN/m)  
öCON3DFö  
/  
CON3DF 4.

2.3

riser

riser

ö ö

"CON3DF".

Phase 2,







3.1.2.

60

- $\frac{W_w}{W_s}$  (w): o %  
 $w\% = (W_w/W_s) \cdot 100$   
 $0 \leq 50\%$ .

- $\frac{V_w}{V_v}$  (s):  
 $S = V_w / V_v$

1 ( 100, %).

- $\frac{W_t}{V_t}$  (b):  
 $b = W_t / V_t$   
 ( )

- $\frac{W_s}{W_s + W_w}$  ( ):  
 $= \frac{W_s}{W_s + W_w}$

- $\frac{W_s + W_w}{V_t}$  (sat):  
 $sat = (W_s + W_w) / V_t$

- $\frac{W_s}{V_t}$  (sub):  
 $sub = sat - w$

3.1

Φαινόμενα βάρη (kN/m <sup>3</sup> ) για ύλες – αργίλους		
sat	d	sub
14-21	6-20	4-12

- \_\_\_\_\_ (e):  
:  
$$e = V_v / V_s$$

e ,

- \_\_\_\_\_ (n):  
$$n(\%) = (V_v / V_t) 100$$

$$e = n / (1 - n)$$

20% 60%.

3.1.5.

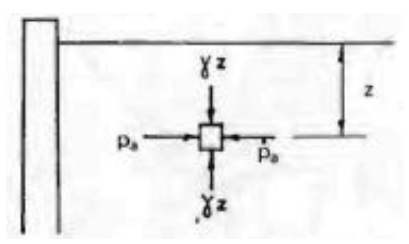
To  $\rho_0 \int_0^z \rho(z) dz = \rho_0 \int_0^z \rho_0 (1 - \beta z) dz$

where  $\rho_0$  is the density at the surface,  $\beta$  is the coefficient of thermal expansion, and  $z$  is the depth. The integral is evaluated as follows:

$$\rho_0 \int_0^z \rho_0 (1 - \beta z) dz = \rho_0^2 \left[ z - \frac{\beta z^2}{2} \right]_0^z = \rho_0^2 \left( z - \frac{\beta z^2}{2} \right)$$

(...)

∴  $v = g z$ ,  
 , g  
 ,  $v = b z$  (3.1.1), b



3.1.1.

$$z_1 < z$$

),

:

$$v\theta = b + (b - w)(z - z_1),$$

w

$$(1025 \text{ kg/m}^3, \quad ).$$

, u.

:

$$v = v\theta + u \quad (\text{Terzaghi, 1920})$$

,  $v\theta$

, u

(, Terzaghi 1923)

### 3.1.5.1.

( . .

.)

).

( ).

(c)

( ).

$$T = N \tan( ) ($$

)

« »-« »  
, c,  
« »

( c).

### 3.1.5.2. ó Mohr-Coulomb.

Mohr.

( ) ( )

$$\begin{aligned} & \text{, } ( \sigma_1 + \sigma_3 ) / 2 \\ ( \sigma_1 - \sigma_3 ) / 2, \quad \sigma_1, \sigma_3 & \quad ( \quad ) \quad \cdot \quad 1 \\ & \quad ( \quad ) \quad 3 \quad ( \quad ) \end{aligned}$$

Mohr.

( 3.1.5),

( , ),

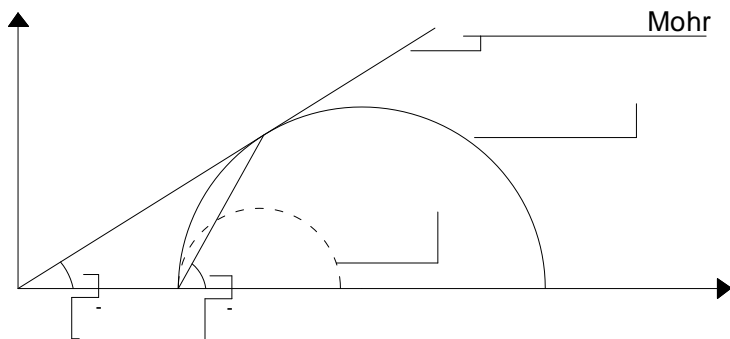
( )

( , )

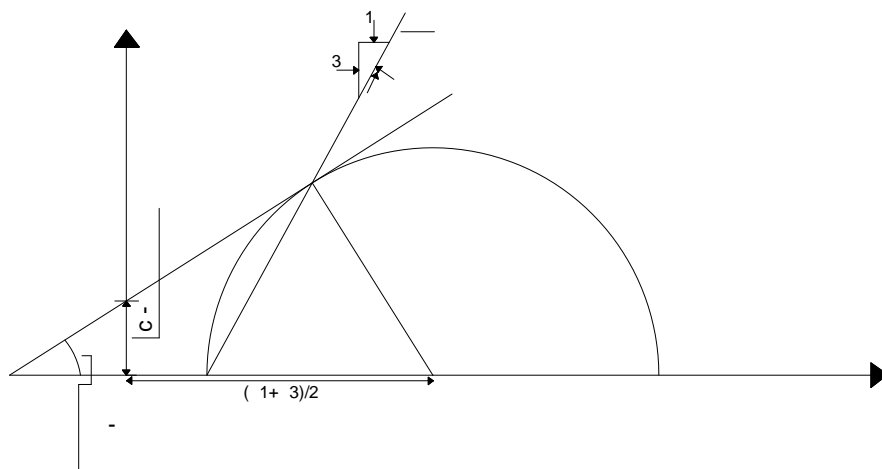
$\tau = \sigma \tan \alpha$  (Coulomb, 1776)

$\tau = \sigma \tan \alpha + c$  (Mohr ó Coulomb)

3.1.5.( )



3.1.5.( )



3.1.5: Mohr

## 3.2

## Phase2

Phase2 Rocscience

```
,
,
,
.
( Mohr-Coulomb, Hoek ó Brown, . . )
.
,
,
( , c,
, Young E, Poisson , .)
(Mohr-Coulomb Hoek-Brown, .).
,
3- , (Uniform)
(Graded),
, 4- , .
( )
,
,
module, "Calculator" Phase2.
module "Interpret"
.
```

### 3.2.1

### Phase2

riser.

#### 3.2.1.1

riser

U, 2.

TDP Phase2,

U, " (Surface excavation element).

3 U

« » :

- (1) ,
- (2) «2/3 »
- (3) «1/3 » .

D=0.429 m,

. , 11

, 0.1 , 0.5 , 1 í 5  
( , , ).

õexcavation elementsö ,

, AutoCAD 2008, format \*.dxf.

ó ,

, . -  
- , ,
















\*.dxf


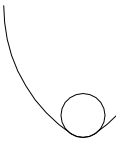

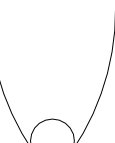
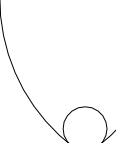
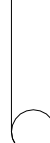


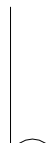
Phase 2,

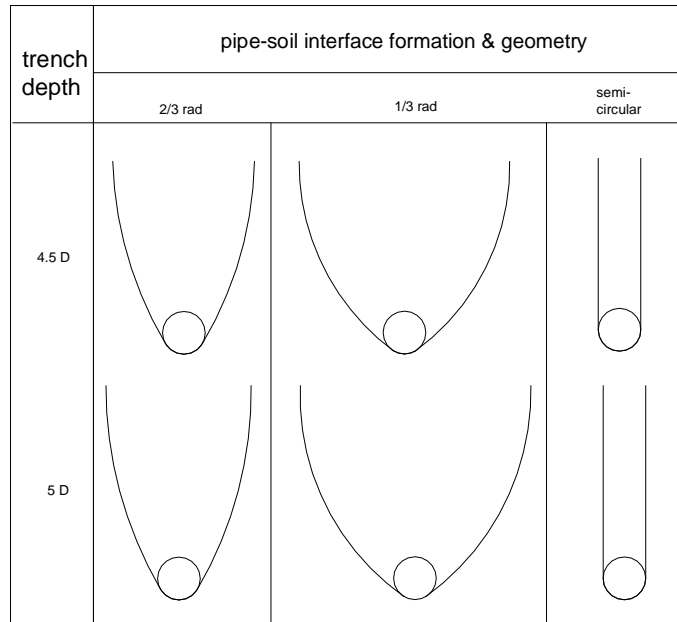


3.2.1.1:

-

trench depth	pipe-soil interface formation & geometry		
	2/3 rad	1/3 rad	semi-circular
0.5 D			
1 D			
1.5 D			
2 D			
2.5 D			

trench depth	pipe-soil interface formation & geometry		
	2/3 rad	1/3 rad	semi-circular
3 D			
3.5 D			
4 D			



**3.2.1.2**

,  
 ( ),  
 ,  
 ,  
 5 ( 2 m)  
 - ,  
 , Mohr-  
 Coulomb.  
 (silty clay soft clay) , Module  $\sigma$  Define  
 Material Properties  $\sigma$  : ) 18 kN/m<sup>3</sup>, ) Young 3000 kPa,  
 ) 0~10 kPa, ) Poisson 0.3, ) 30  
 ) 15 kPa.

riser,

TDP,

(Loose sand Sandy

Clay) : ) 16 kN/m<sup>3</sup>, )

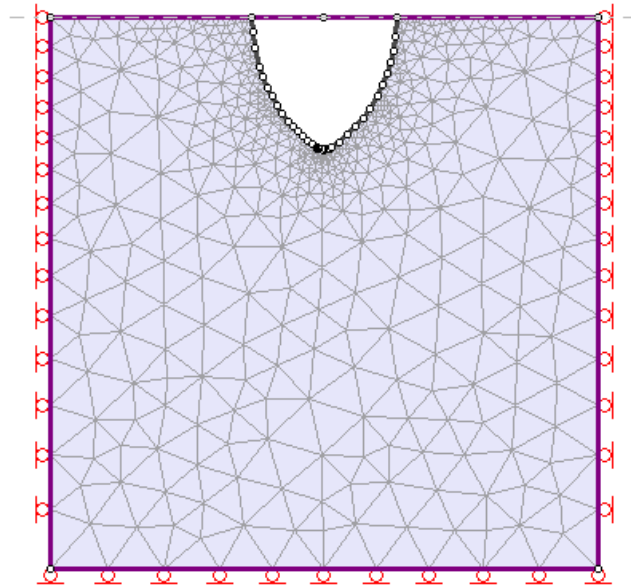
Young 20000 kPa, ) 0 kPa, ) Poisson 0.3, )

40 ) 15 kPa.

**3.2.1.3**

3-

(Graded)  
( . 3.2.1.3).



3.2.1.3:

1/3

### 3.2.1.4.

Phase2  
,  
øbolt elementsö,  
/ øliner elementsö,  
riser ( ),  
øboltsö.  
ø ó ö  
2,  
riser. riser  
riser

### 3.2.1.5.

ø -  
"Elastic"  
ó

a priori

ó

riser

### 3.3

### Phase 2

Phase 2

Coulomb"

"Mohr-

1, 3

3.1.

riser,

xx, yy, xy

O

module "Calculate"

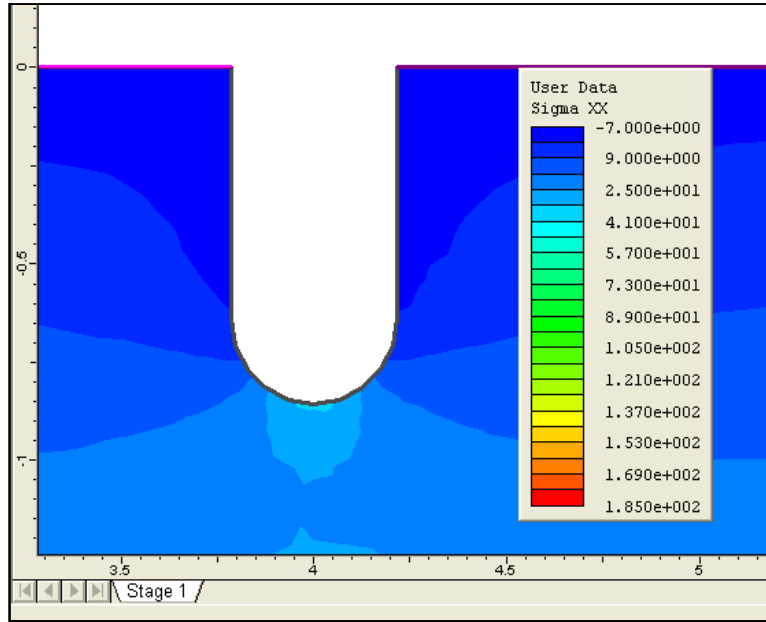
3.2.

module "Interpret"

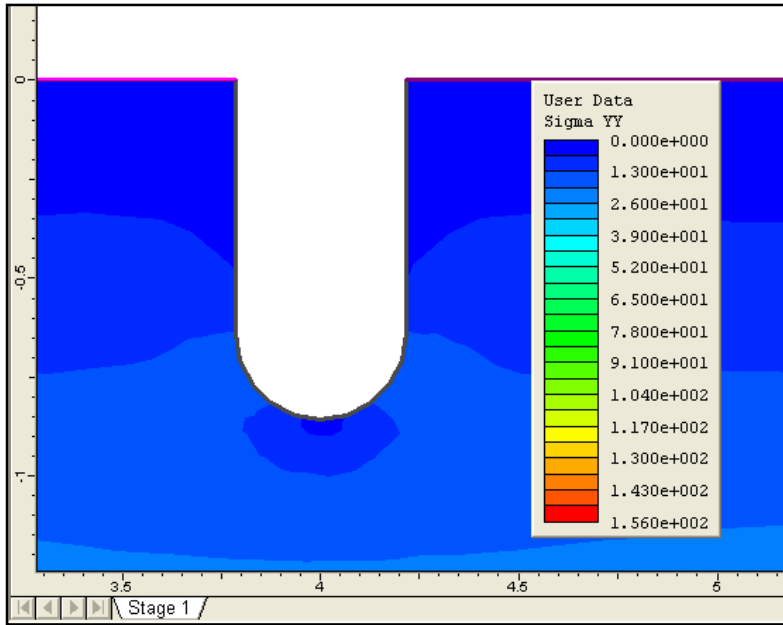
"Legend plots"

" " " - " (soft clay).

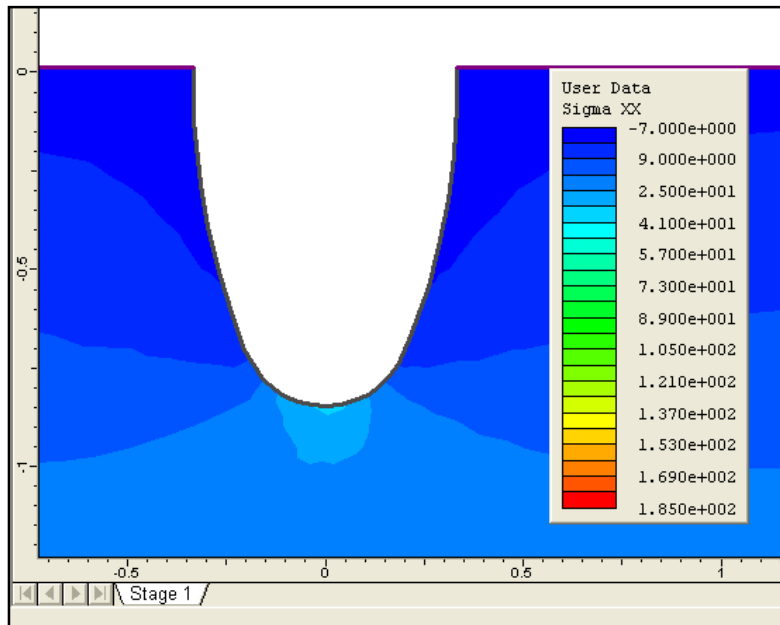
kPa:



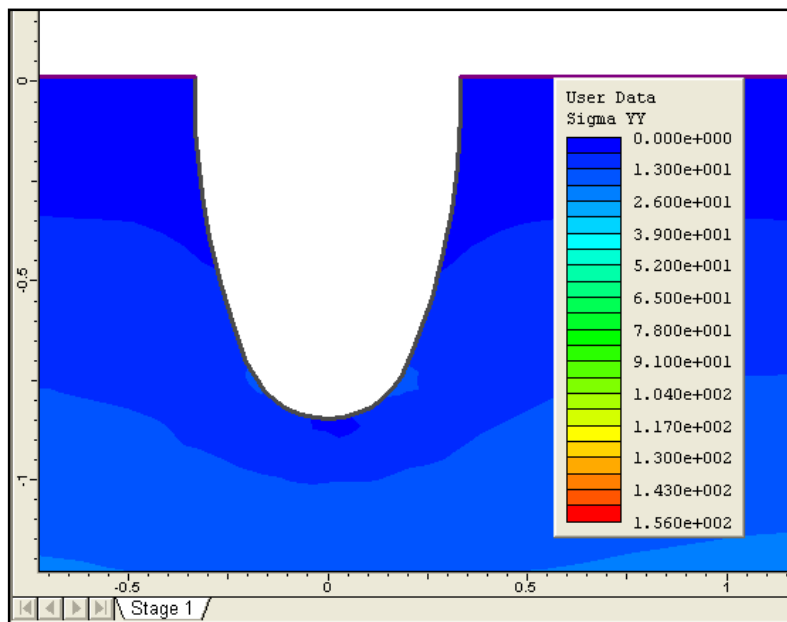
. 3.3.1: riser- xx 2D.



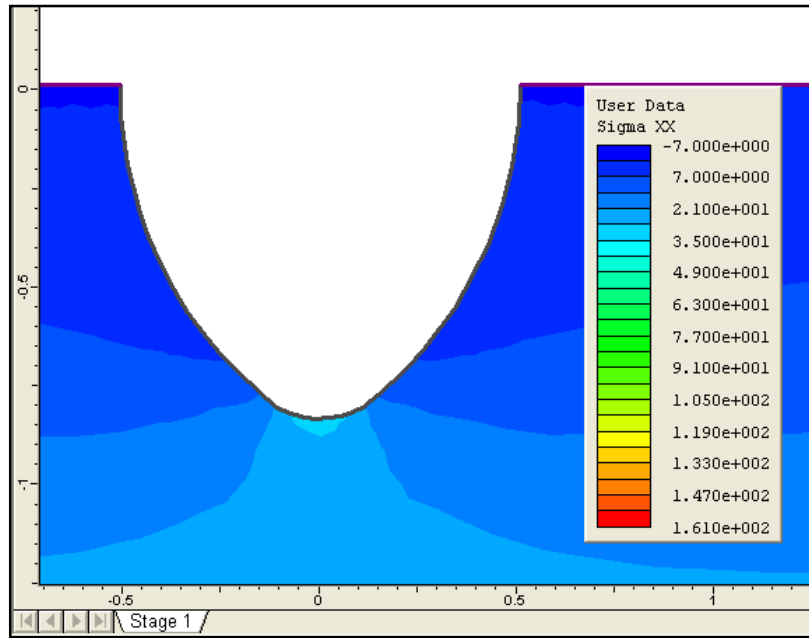
. 3.3.2: riser- yy 2D.



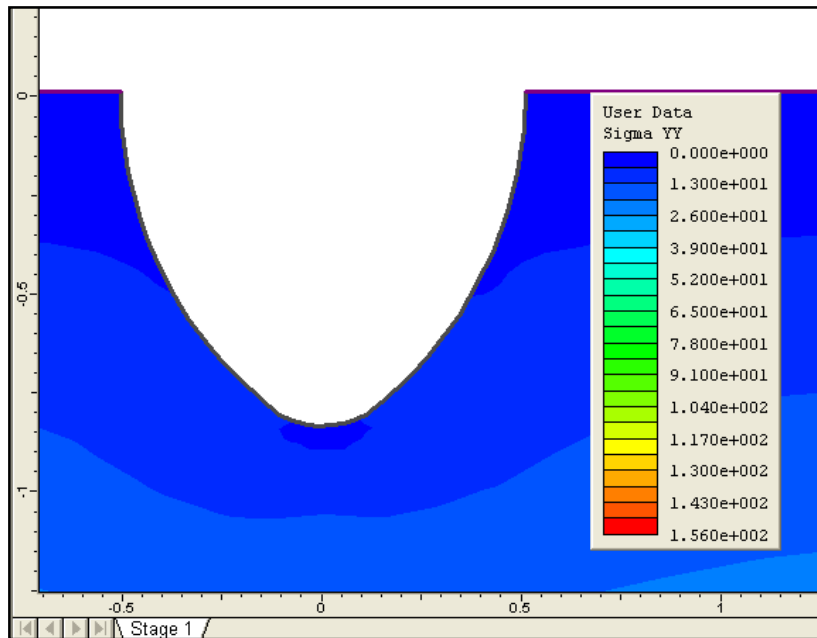
. 3.3.3:  $2R/3$   $xx$  - riser-2D.



. 3.3.4:  $2R/3$   $yy$  - riser-2D.



. 3.3.5:  $R/3$   $xx$  - riser-2D.



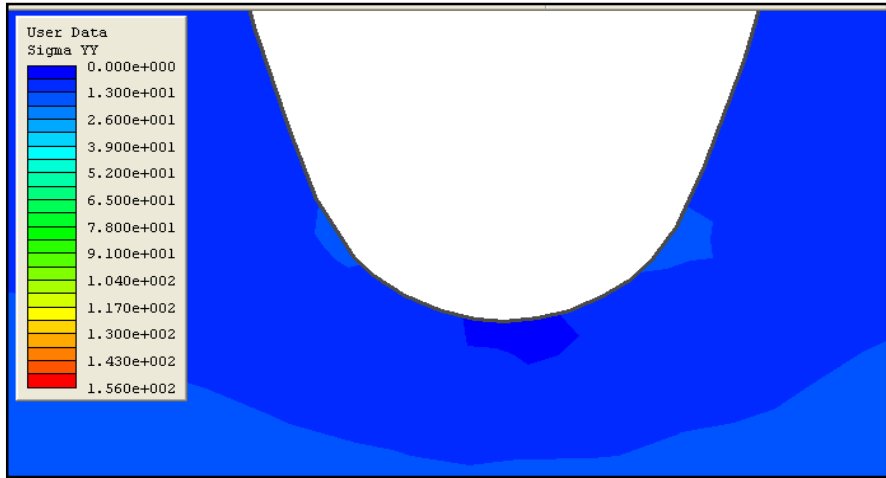
. 3.3.6:  $R/3$   $yy$  - riser-2D.



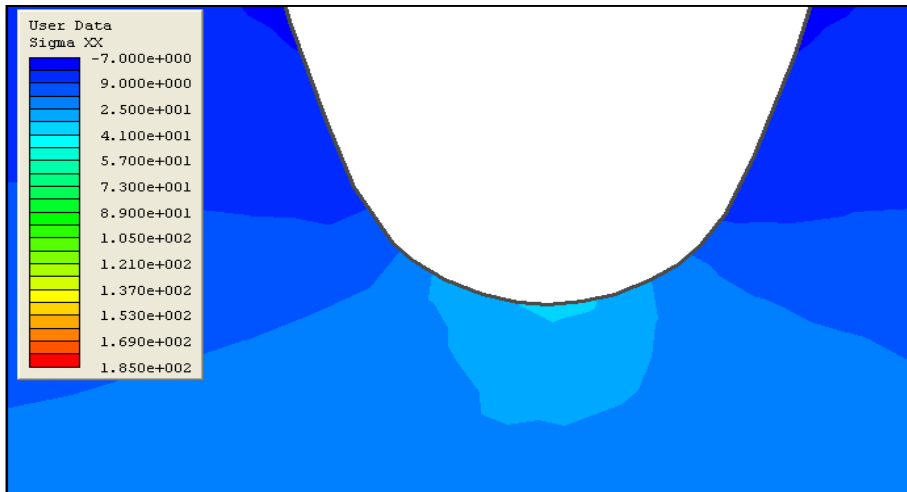
```

      ,
      . , -
      ( R/3 --> 2R/3 --> )
      ,
      ,
      yy 2 ,
      xx
      ,
      ,
      riser. , yy
      zz (vertical), xx yy (out-of-plane) xx (In-
plane)
      , 2D ,
      , (x-z). , ,
      ,
      .
      "Legend plots" module
"Interpret", - riser-
      :

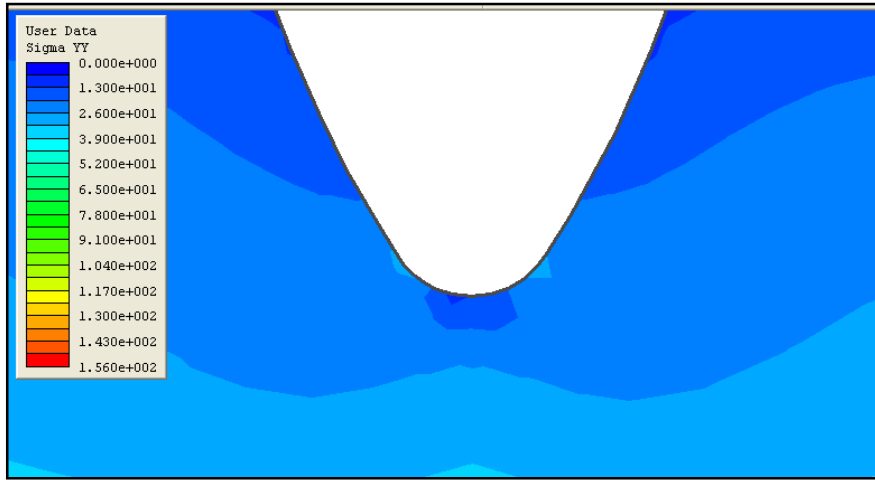
```



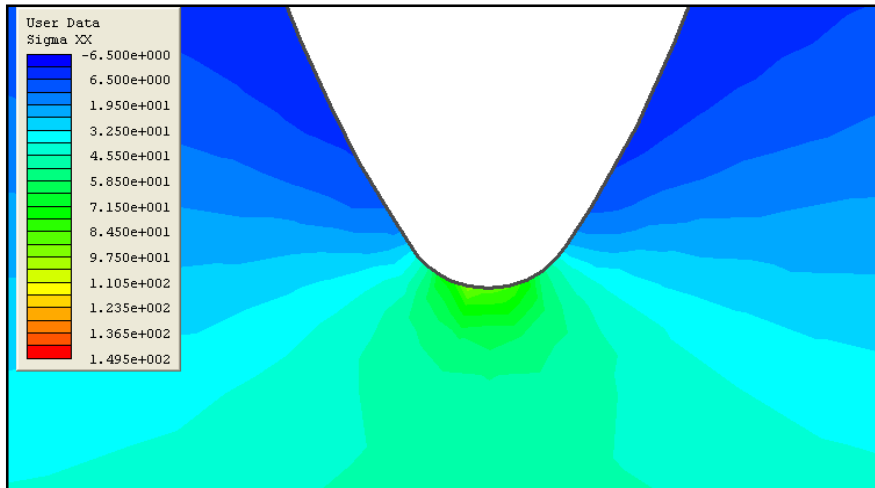
. 3.3.7:  $2 R / 3$   $yy$  - riser-2D.



. 3.3.8:  $2 R / 3$   $xx$  - riser-2D.



. 3.3.9:  $yy$  - riser-  
 $2 R / 3$  4D.



. 3.3.10:  $xx$  - riser-  
 $2 R / 3$  4D.

### 3.4

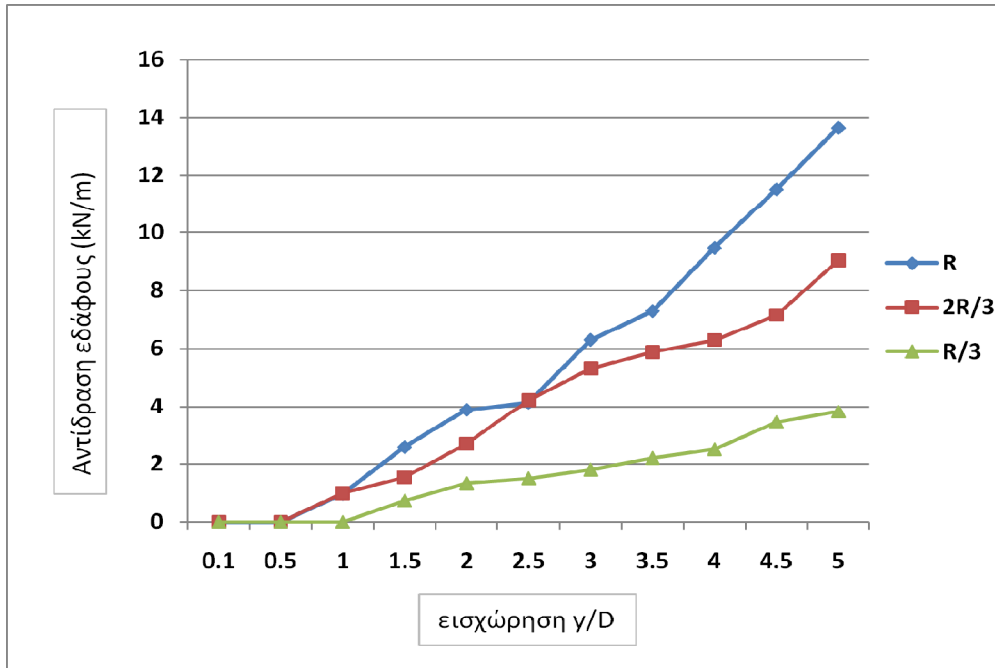
- $n$  ,  $1, 2$  ,  $R = 0.2145$   
 $m$ ,  $d = (r_2 - r_1)/(n-1)$ .  
 $i$  ,  $i = 1, 2, \dots, n$   
 $i = 1 + (i-1)d$
- $i$   $i = -x_{x,i} \cos i - y_{y,i} \sin i$ ,  
 $x_{x,i}$ ,  $y_{y,i}$
- $c = 1$   $i \in [2, n-1]$ ,  $c = 1/2$   $i = 1$   $c = 1/2$   $i = n$
- 

$$F_z = - \sum_{i=1}^n R c_i i \sin i d$$

Matlab.

"script"

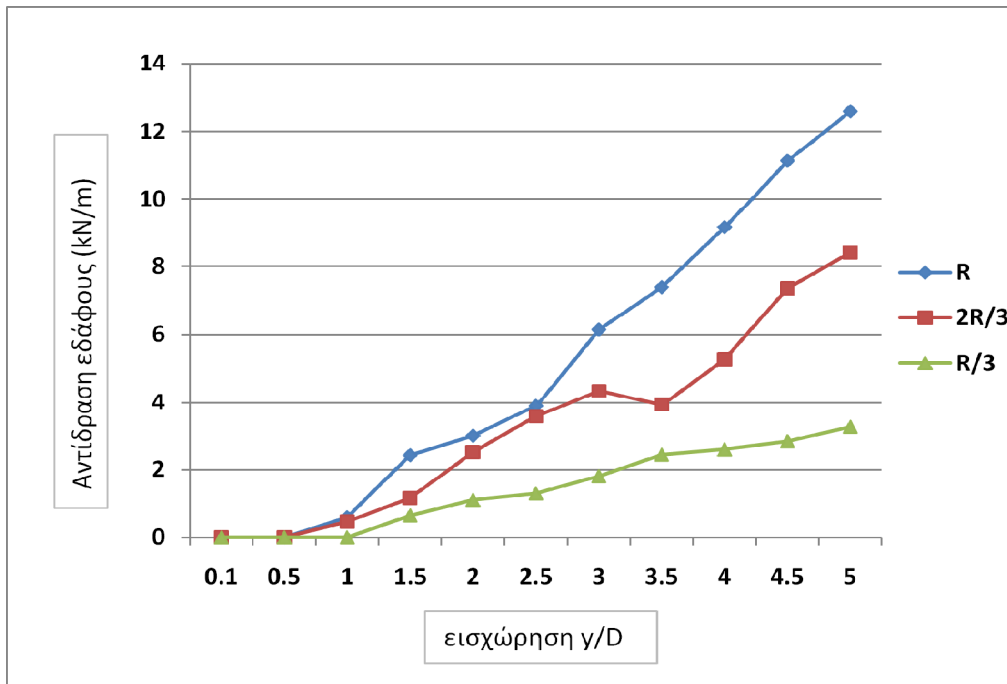
(R/3 --> 2R/3 --> R).



3.4.1:

riser

-



3.4.2:

riser

-

, <D,

Phase 2

( )

y: [2D, 2.5D]

R 2R/3,



4.

riser

CON3DF

TDP.

4.1.

riser [7],

(Lagrangian)

Lagrangian, s.

, s=0

riser

, s=L,

, L

riser.

riser

:

•

•

•

•

•

$EA/L$

•

ó « »

•



riser

:

- 
- 
- ( . . .  
Chatjigeorgiou, *A finite differences formulation for the linear and nonlinear dynamics of 2D catenary risers*, *Ocean Engineering*, 2008)
- riser,
- ó
- riser

#### 4.1.1.

riser

:

- ,
- $m$ , riser
- $m_a$
- $w_o$ , riser
- $d_o$
- ,
- $I_p$ ,
- $I$ ,
- $\epsilon$
- $E$ , Young
- $G$ ,

To

riser

:

$$dp = ds(1+e), \quad (1)$$

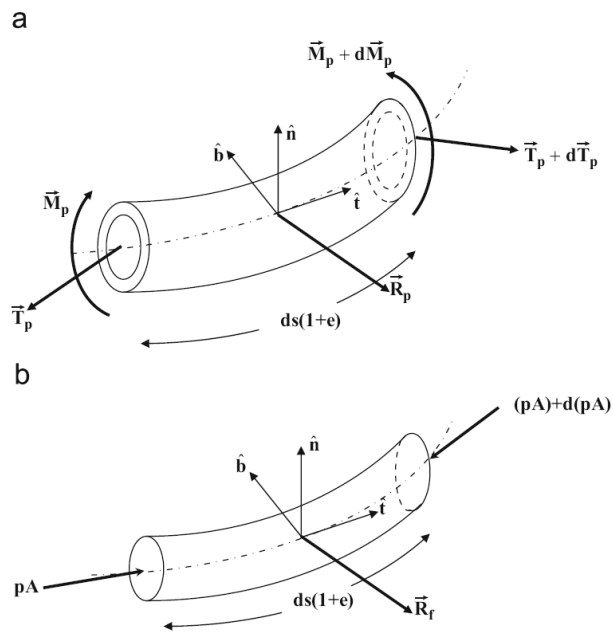
ds

, e

s

( 4.1.1.).

,  $\vec{t}, \vec{n}, \vec{b}$



4.1.1.

a.

riser

b.

riser

:

$$\vec{T}_p = T\vec{t} + S_n\vec{n} + S_b\vec{b}$$

$$\vec{M}_p = M_1\vec{t} + M_2\vec{n} + M_3\vec{b} \tag{2}$$

T, S<sub>b</sub> (in-plane), S<sub>n</sub> (out-of-plane), M<sub>1</sub> (in-plane), M<sub>2</sub> (out-of-plane), M<sub>3</sub> (riser in-plane), pA $\vec{t}$  4.1.1.b.

, , , :

$$\sum \vec{R}_p = \vec{R}_{pw} + \vec{R}_{pa} + \vec{R}_{pd} \tag{3}$$

$$\sum \vec{R}_f = \vec{R}_{fw} \tag{4}$$

R<sub>pw</sub>, R<sub>pa</sub>, R<sub>pd</sub>

4.1.2.

Langrangian

$\vec{G}$ :

$$\vec{G} = G_1 \vec{t} + G_2 \vec{n} + G_3 \vec{b} \quad (5)$$

$$\frac{D\vec{G}}{Ds} = \frac{\partial \vec{G}}{\partial s} + G_1 \frac{\partial \vec{t}}{\partial s} + G_2 \frac{\partial \vec{n}}{\partial s} + G_3 \frac{\partial \vec{b}}{\partial s} \quad (6)$$

Darboux,  $\vec{\Omega}$ ,

$$\vec{\Omega} = \Omega_1 \vec{t} + \Omega_2 \vec{n} + \Omega_3 \vec{b}. \quad (7)$$

Darboux (M.S. Rahman, 1994),

$$\frac{\partial \vec{t}}{\partial s} = \vec{\Omega} \times \vec{t}, \quad \frac{\partial \vec{n}}{\partial s} = \vec{\Omega} \times \vec{n}, \quad \frac{\partial \vec{b}}{\partial s} = \vec{\Omega} \times \vec{b}$$

$\vec{G}$  :

$$\frac{D\vec{G}}{Ds} = \frac{\partial \vec{G}}{\partial s} + \vec{\Omega} \times \vec{G} \quad (8)$$

$\vec{G}$ ,

Darboux

,  $\vec{\omega}$ :

$$\vec{\omega} = \omega_1 \vec{t} + \omega_2 \vec{n} + \omega_3 \vec{b}, \quad (9)$$

1, 2, 3

 $\vec{G}$ ,

:

$$\frac{D\vec{G}}{Dt} = \frac{\partial \vec{G}}{\partial t} + \vec{\omega} \times \vec{G} \quad (10)$$

 $\vec{\omega}$      $\vec{\Omega}$ 

Euler,

[21, 22]

:

$$\omega_1 = \frac{\partial \psi}{\partial t} - \frac{\partial \phi}{\partial t} \sin \theta$$

$$\omega_2 = \frac{\partial \theta}{\partial t} \cos \psi + \frac{\partial \phi}{\partial t} \cos \theta \sin \psi$$

$$\omega_3 = \frac{\partial \phi}{\partial t} \cos \theta \cos \psi - \frac{\partial \theta}{\partial t} \sin \psi$$

$$\Omega_1 = \frac{\partial \psi}{\partial s} - \frac{\partial \phi}{\partial s} \sin \theta$$

(11)

$$\Omega_2 = \frac{\partial \theta}{\partial s} \cos \psi + \frac{\partial \phi}{\partial s} \cos \theta \sin \psi$$

$$\Omega_3 = \frac{\partial \phi}{\partial s} \cos \theta \cos \psi - \frac{\partial \theta}{\partial s} \sin \psi$$

,  
:

$$\vec{M}_p = M_1 \vec{t} + M_2 \vec{n} + M_3 \vec{b} = GI_p \Omega_1 \vec{t} + EI \Omega_2 \vec{n} + EI \Omega_3 \vec{b} \quad (12)$$

### 4.1.3.

#### 4.1.3.1.

Newton

:

$$m \frac{D\vec{V}_p}{Dt} = \frac{D\vec{T}_p}{Ds} + \sum \vec{R}_p (1+e) \quad (13)$$

,  
:

$$m \left( \frac{\partial \vec{V}_p}{\partial t} + \vec{\omega} \times \vec{V}_p \right) = \frac{\partial \vec{T}_p}{\partial s} + \vec{\Omega} \times \vec{T}_p + (\vec{R}_{pw} + \vec{R}_{pa} + \vec{R}_{pd})(1+e), \quad (14)$$

$\vec{V}_p$

,

$$\vec{V}_p = u \vec{t} + v \vec{n} + w \vec{b}.$$

4.1.3.2.

[22]:

$$\frac{1}{1+e} \frac{D}{Dt} [\rho_c I \vec{\omega}] = \frac{1}{(1+e)^2} \frac{D\vec{M}_p}{Ds} + \vec{t} \times \vec{T}_p (1+e) \quad (15)$$

3X3 (cI<sub>p</sub>, cI, cI),

$$\frac{\rho_c I}{1+e} \left( \frac{\partial \vec{\omega}}{\partial t} + \vec{\omega} \times \vec{\omega} \right) = \frac{1}{(1+e)^2} \left( \frac{\partial \vec{M}_p}{\partial s} + \vec{\Omega} \times \vec{M}_p \right) + \vec{t} \times \vec{T}_p (1+e) \quad (16)$$

4.1.3.3.

$\vec{r}(s, t)$ ,

, s t,

$$\frac{D}{Dt} \left[ \frac{D\vec{r}}{Ds} \right] = \frac{D}{Ds} \left[ \frac{D\vec{r}}{Dt} \right] \quad (17)$$

4.1.1.a:

$$\frac{D\vec{r}}{Ds} = (1+e)\vec{t} \quad \frac{D\vec{r}}{Dt} = \vec{V}_p$$

,  $\dot{\phi}$ ,  $e = T/EA$ ,  
:

$$\frac{1}{EA} \frac{\partial T}{\partial t} \vec{t} + (1+e)\vec{\omega} \times \vec{t} = \frac{\partial \vec{V}_p}{\partial s} + \vec{\Omega} \times \vec{V}_p \quad (18)$$

#### 4.1.4

##### 4.1.4.1.

4.1.1.b. :

$$M \frac{D\vec{V}_f}{Dt} = \frac{D(-pA\vec{t})}{Ds} + \sum \vec{R}_f (1+e) \quad (19)$$

$$\vec{V}_f = U\vec{t} + v\vec{n} + w\vec{b}$$

,  $\dot{\phi}$  .

$$m \left( \frac{\partial \vec{V}_f}{\partial t} + \vec{\omega} \times \vec{V}_f \right) = \frac{\partial (-pA\vec{t})}{\partial s} + \vec{\Omega} \times (-pA\vec{t}) + \vec{R}_{fw} (1+e) \quad (20)$$



4.1.4.2.

$$\frac{D}{Dt}[(1+e)\vec{t}] = \frac{D\vec{V}_f}{Ds} \quad (21)$$

4.1.1.b.

$$(1+e)\vec{\omega} \times \vec{t} = \frac{\partial \vec{V}_f}{\partial s} + \vec{\Omega} \times \vec{V}_f + \frac{1}{EA} \frac{\partial pA}{\partial t} \vec{t} \quad (22)$$

$$\frac{1}{EA} \frac{\partial pA}{\partial t} \vec{t}$$

4.1.5

(14), (16), (18), (20), (22).

$$(22) \quad (20)$$

:

$$m \frac{\partial \vec{V}_f}{\partial t} + \frac{MU}{1+e} \left( \frac{\partial \vec{V}_f}{\partial s} + \vec{\Omega} \times \vec{V}_f + \frac{1}{EA} \frac{\partial pA}{\partial t} \vec{t} \right) + M(v^* \vec{\omega} \times \vec{n} + w^* \vec{\omega} \times \vec{b}) =$$

$$-\frac{\partial pA}{\partial t} \vec{t} - pA^* \vec{\Omega} \times \vec{t} + \vec{R}_{fw}(1+e), \quad (23)$$

,

$$(14) \quad (23)$$

:

$$m \left( \frac{\partial \vec{V}_p}{\partial t} + \vec{\omega} \times \vec{V}_p \right) + M \frac{\partial \vec{V}_f}{\partial t} + \frac{MU}{1+e} \left( \frac{\partial \vec{V}_f}{\partial s} + \vec{\Omega} \times \vec{V}_f + \frac{1}{EA} \frac{\partial pA}{\partial t} \vec{t} \right) +$$

$$M(v^* \vec{\omega} \times \vec{n} + w^* \vec{\omega} \times \vec{b}) = \frac{\partial T_p}{\partial s} + \Omega \times T_p - \frac{\partial pA}{\partial s} \vec{t} - pA \Omega \times \vec{t} +$$

$$(\vec{R}_{pw} + \vec{R}_{fw} + \vec{R}_{pa} + \vec{R}_{pd})(1+e), \quad (24)$$

#### 4.1.6

$$(16), (18) \quad (24),$$

:

$$(\vec{R}_{pw} + \vec{R}_{fw})(1+e) = -(w_o + Mg) \sin \phi \cos \theta^* \vec{t} - (w_o + Mg) \cos \psi^* \vec{n} -$$

$$(w_o + Mg) \sin \phi \sin \theta^* \vec{b}$$

$$\vec{R}_{pa}(1+e) = -m_a \frac{\partial V_{2r}}{\partial t} \vec{n} - m_a \frac{\partial V_{3r}}{\partial t} \vec{b}$$

$$\vec{R}_{pd}(1+e) = R_{dt} \vec{t} + R_{dn} \vec{n} + R_{db} \vec{b}$$

$$\begin{aligned}
R_{dt} &= -1/2 \rho d_o C_{dt} u_{1r} |u_{1r}| \sqrt{1+e} \\
R_{dn} &= -1/2 \rho d_o C_{dn} u_{2r} \sqrt{u_{2r}^2 + u_{3r}^2} \sqrt{1+e} \\
R_{db} &= -1/2 \rho d_o C_{db} u_{3r} \sqrt{u_{2r}^2 + u_{3r}^2} \sqrt{1+e}, \tag{25}
\end{aligned}$$

g  
( ), u<sub>1r</sub>, u<sub>2r</sub>, u<sub>3r</sub>  
( u, v, w). R<sub>dt</sub>, R<sub>dn</sub>, R<sub>db</sub>  
, Morison C<sub>dt</sub>, C<sub>dn</sub>, C<sub>db</sub>

#### 4.1.7

(16), (18) (24), :

•

:

$$\begin{aligned}
m \frac{\partial u}{\partial t} + (M+m)(\omega_2 w - \omega_3 v) + M \frac{dU}{dt} + \frac{MU}{1+e} (\Omega_2 w - \Omega_3 v + \frac{1}{EA} \frac{\partial pA}{\partial t}) = \\
\frac{\partial(T-pA)}{\partial s} + S_b \Omega_2 - S_n \Omega_3 - (w_o + Mg) \sin \phi \cos \theta + R_{dt} \tag{26}
\end{aligned}$$

$$\begin{aligned}
(m+M) \frac{\partial v}{\partial t} + m(\omega_3 u - \omega_1 w) + M \omega_1 w + \frac{MU}{1+e} \frac{\partial v}{\partial s} + \frac{MU^2}{1+e} \Omega_3 - \frac{MU}{1+e} \Omega_1 w + \\
m_a \frac{\partial v_{2r}}{\partial t} = \frac{\partial S_n}{\partial s} + \Omega_3 (T-pA) - \Omega_1 S_b - (w_o + Mg) \cos \phi + R_{dn} \tag{27}
\end{aligned}$$

$$(m + M) \frac{\partial w}{\partial t} + m(\omega_1 v - \omega_2 u) + M\omega_1 v + \frac{MU}{1+e} \frac{\partial w}{\partial s} + \frac{MU^2}{1+e} \Omega_2 - \frac{MU}{1+e} \Omega_1 v + m_a \frac{\partial v_{3r}}{\partial t} = \frac{\partial S_b}{\partial s} - \Omega_2(T - pA) + \Omega_1 S_n - (w_o + Mg) \sin \phi \sin \theta + R_{db} \quad (28)$$

•

$$\frac{1}{EA} \frac{\partial T}{\partial t} = \frac{\partial u}{\partial s} + \Omega_2 w - \Omega_3 v \quad (29)$$

$$(1+e)\omega_3 = \frac{\partial v}{\partial s} + \Omega_3 u - \Omega_1 w \quad (30)$$

$$-(1+e)\omega_2 = \frac{\partial w}{\partial s} + \Omega_1 v - \Omega_2 u \quad (31)$$

•

$$(1+e)\rho_c I_p \frac{\partial \omega_1}{\partial t} = GI_p \frac{\partial \Omega_1}{\partial s} \quad (32)$$

$$(1+e)\rho_c I \frac{\partial \omega_2}{\partial t} = EI \frac{\partial \Omega_2}{\partial s} + (GI_p - EI)\Omega_1 \Omega_3 - S_b(1+e)^3 \quad (33)$$

$$(1+e)\rho_c I \frac{\partial \omega_3}{\partial t} = EI \frac{\partial \Omega_3}{\partial s} + (EI - GI_p)\Omega_1 \Omega_2 - S_n(1+e)^3 \quad (34)$$

(32) (34)

$GI_p$

s.

(26-34)

9

13

,

:

$T, pA, S_n, S_b, u, v, w, \omega_1, \omega_2, \omega_3, \Omega_1, \Omega_2, \Omega_3$

Euler, , , . ,

(26-34) 3

(11)



$$\begin{aligned} & \frac{\partial T_e}{\partial s} + S_b \Omega_2 - S_n \Omega_3 - (w_o + Mg) \sin \phi \cos \theta + R_{dt} - m \frac{\partial u}{\partial t} \\ & - (m + M) \left( w \frac{\partial \theta}{\partial t} - v \frac{\partial \phi}{\partial t} \cos \theta \right) - \frac{MU}{1+e} (\Omega_2 w - \Omega_3 v) = 0 \end{aligned} \quad (35)$$

$$\begin{aligned} & \frac{\partial S_n}{\partial s} + \Omega_3 (T_e - S_b \tan \theta) - (w_o + Mg) \cos \phi + R_{dn} - (m + M) \frac{\partial v}{\partial t} \\ & - m \frac{\partial \phi}{\partial t} (u \cos \theta + w \sin \theta) - Mw \frac{\partial \phi}{\partial t} \sin \theta - \frac{MU}{1+e} \frac{\partial u}{\partial s} - \frac{MU^2}{1+e} \Omega_3 \\ & - \frac{MU}{1+e} w \Omega_3 \tan \theta - m_a \frac{\partial v}{\partial t} = 0 \end{aligned} \quad (36)$$

$$\begin{aligned} & \frac{\partial S_b}{\partial s} - \Omega_2 T_e - \Omega_3 S_n \tan \theta - (w_o + Mg) \sin \phi \sin \theta + R_{db} - (m + M) \frac{\partial w}{\partial t} \\ & - m \left( \frac{\partial \phi}{\partial t} v \sin \theta + u \frac{\partial \theta}{\partial t} \right) - Mv \frac{\partial \phi}{\partial t} \sin \theta - \frac{MU}{1+e} \frac{\partial w}{\partial s} + \frac{MU^2}{1+e} \Omega_2 \\ & + \frac{MU}{1+e} v \Omega_3 \tan \theta - m_a \frac{\partial w}{\partial t} = 0 \end{aligned} \quad (37)$$

$$\frac{\partial u}{\partial s} + \Omega_2 w - \Omega_3 v - \frac{1}{EA} \frac{\partial T_e}{\partial t} = 0 \quad (38)$$

$$\frac{\partial v}{\partial s} + \Omega_3 (u + w \tan \theta) - (1+e) \frac{\partial \phi}{\partial t} \cos \theta = 0 \quad (39)$$

$$\frac{\partial w}{\partial s} + \Omega_3 v \tan \theta - \Omega_2 u + (1+e) \frac{\partial \theta}{\partial t} = 0 \quad (40)$$

$$EI \frac{\partial \Omega_2}{\partial s} + EI \Omega_3^2 \tan \theta - S_b (1+e)^3 = 0 \quad (41)$$

$$EI \frac{\partial \Omega_3}{\partial s} - EI \Omega_3 \Omega_2 \tan \theta + S_n (1+e)^3 = 0 \quad (42)$$

$$\frac{\partial \theta}{\partial s} - \Omega_2 = 0 \quad (43)$$

$$\frac{\partial \phi}{\partial s} \cos \psi - \Omega_3 = 0 \quad (44)$$

4.1.8

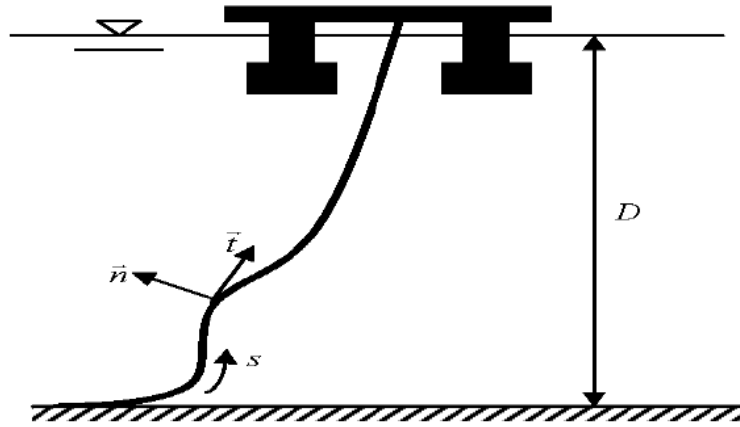
riser

:

e T/EA,

x-z (in-plane)

4.1.6.:



4.1.6.:

riser

x-z

$$\frac{\partial T}{\partial s} - S_n \Omega_3 - w_o \sin \phi \cos \theta + R_{dt} - m \left( \frac{\partial u}{\partial t} - v \frac{\partial \phi}{\partial t} \right) = 0 \quad (45)$$

$$\frac{\partial S_n}{\partial s} + \Omega_3 T - w_o \cos \phi + R_{dn} - m \left( \frac{\partial v}{\partial t} + u \frac{\partial \phi}{\partial t} \right) - m_a \frac{\partial v}{\partial t} = 0 \quad (46)$$

$$EI \frac{\partial \Omega_3}{\partial s} + S_n \left( 1 + \frac{T}{EA} \right)^3 = 0 \quad (47)$$

$$\frac{\partial u}{\partial s} - \Omega_3 v - \frac{1}{EA} \frac{\partial T}{\partial t} = 0 \quad (48)$$

$$\frac{\partial v}{\partial s} + \Omega_3 u - \left(1 + \frac{T}{EA}\right) \frac{\partial \phi}{\partial t} = 0 \quad (49)$$

$$\frac{\partial \phi}{\partial s} - \Omega_3 = 0 \quad (50)$$

## 4.2

, .

• Box Methodö (Box and Keller)

Chatjigeorgiou [7, 12, 31], Chatjigeorgiou and Mavrakos [28, 29], Tjavaras et al. [40], Howell [22] . . .

(s, t)

n

. :

• :

$$\mathbf{M} \frac{\partial \mathbf{Y}}{\partial t} + \mathbf{K} \frac{\partial \mathbf{Y}}{\partial s} + \mathbf{F}(\mathbf{Y}, s, t) = \mathbf{0}$$

• ( ) :

$$Y = [T \quad S_n \quad u \quad v \quad \Omega_3 \quad \phi]^T$$

• H  
• Box Methodö :



$$\begin{aligned}
& (M_k^{i+1} + M_k^i) \left( \frac{Y_k^{i+1} - Y_k^i}{\Delta t} \right) + (M_{k-1}^{i+1} + M_{k-1}^i) \left( \frac{Y_{k-1}^{i+1} - Y_{k-1}^i}{\Delta t} \right) + \\
& (K_{k-1}^{i+1} + K_k^{i+1}) \left( \frac{Y_k^{i+1} - Y_{k-1}^{i+1}}{\Delta s} \right) + (K_{k-1}^i + K_k^i) \left( \frac{Y_k^i - Y_{k-1}^i}{\Delta s} \right) \\
& + (F_k^{i+1} + F_{k-1}^{i+1} + F_k^i + F_{k-1}^i) = 0
\end{aligned}$$

k (s) i  
(t), M, F K

Chatjigeorgiou [7].

,  
riser,  
Larsen Passano [11] Chatjigeorgiou [7]  
:

, L (m)	2024
, D (m)	0.429
, d <sub>i</sub> (m)	0.385
, m (kg/m)	262.933
, C <sub>a</sub>	1.0
, w <sub>o</sub> (N/m)	927.4
, EA (N)	0.5823x10 <sup>10</sup>
, EI (Nm <sup>2</sup> )	0.1209x10 <sup>9</sup>
. / , C <sub>dn</sub>	1.0
. / , C <sub>dt</sub>	0.0
, d (m)	1800
, T <sub>p</sub> (kN)	1860

2  
 z ó heave , 1 m, x - surge  
 , = 0.2, 0.4, 0.6, 0.8, 1.0 rad/sec. 5

H  
 , t = 1 sec , 2 rad/sec t = 0.2  
 sec , 1 rad/sec n = 400 .



5.  
Riser

CON3DF.

Steel Catenary

5.1

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, (TDP),

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TDP

TDP

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TDP

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• TDP riser. ,  
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, TDP

• TDP.  
, TDP.

• TDP s,

riser , CON3DF.f,  
FORTRAN . . .

) ,  
:

) TDP  
 ) , TDP.  
 ö δ  
 3.

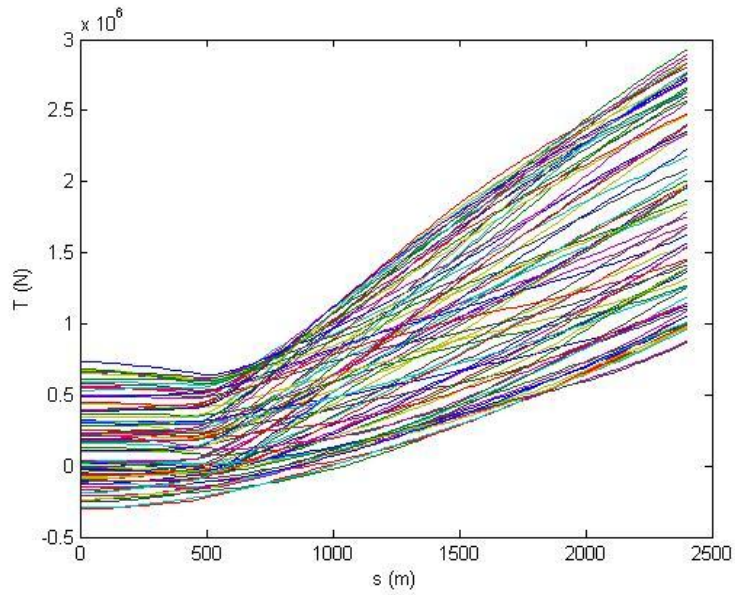
**5.2 CON3DF.**

( riser  
 heave/surge),  
 Langrangian, s  
 t, 2  
 Riser- , 2R/3 2 , 2D 2.5D.  
 2696 N/m 4226 /m, - , 2515 /m 3575  
 N/m,  
 heave 1 m (x=0 z=1)  
 =1.0 rad/sec , surge  
 (x=1 z=0)  
 1 m/sec,

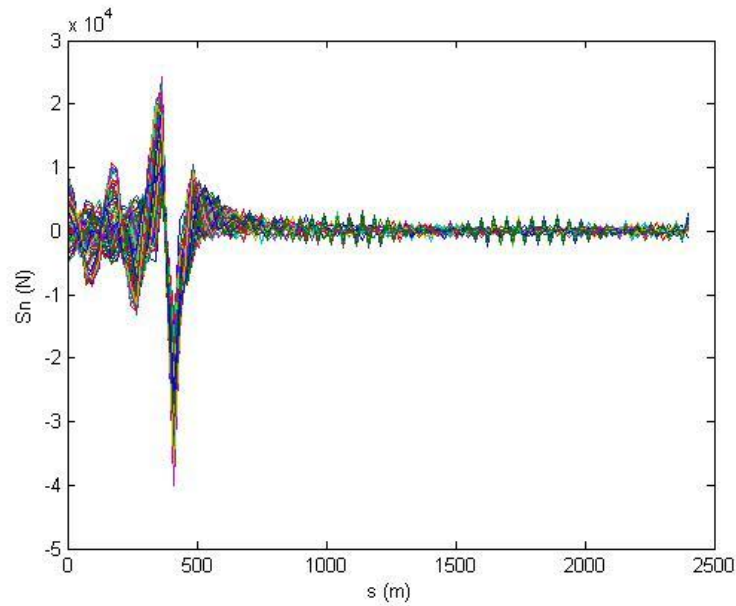
TDP  
 Chatjigeorgiou, Passano  
 and Larsen [12] Simos and Fujjara [14].

5.1.1 - 5.1.4:

\_\_\_\_\_ , s, \_\_\_\_\_  
 \_\_\_\_\_ heave 1 m: \_\_\_\_\_



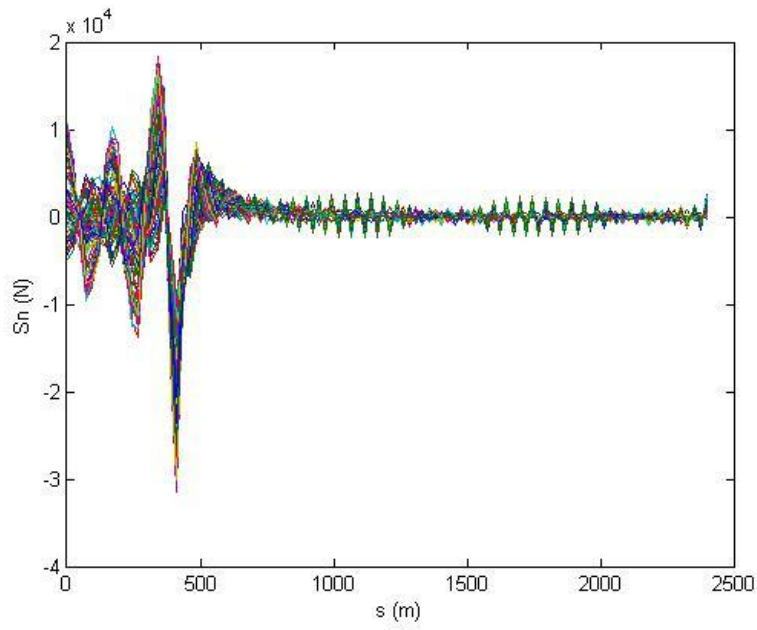
5.1.1. T 1 rad/s. 1 m  
 - TDP 3575 N/m



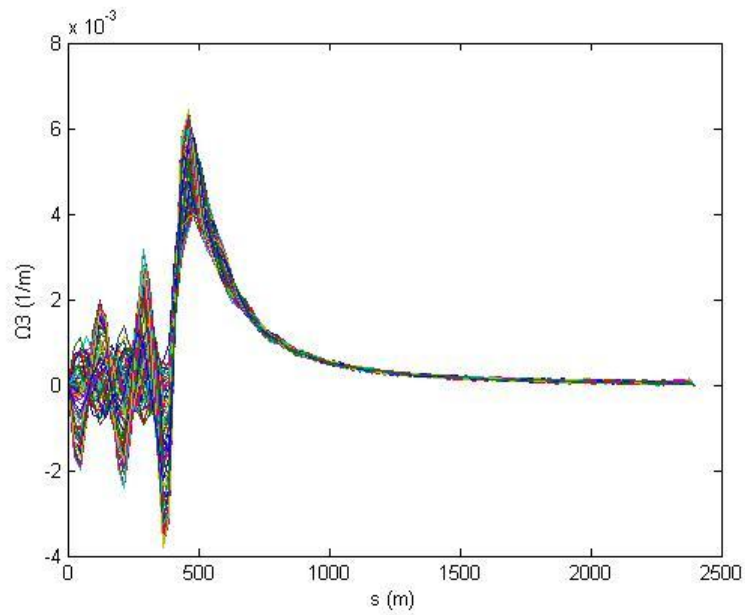
5.1.1. Sn 1 rad/s. 1 m  
 m - TDP 3575 N/m



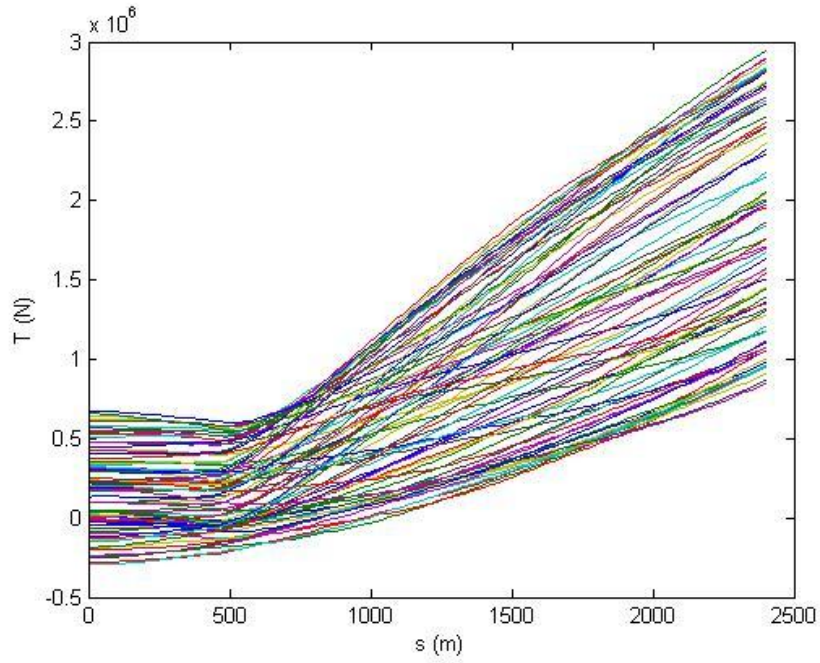




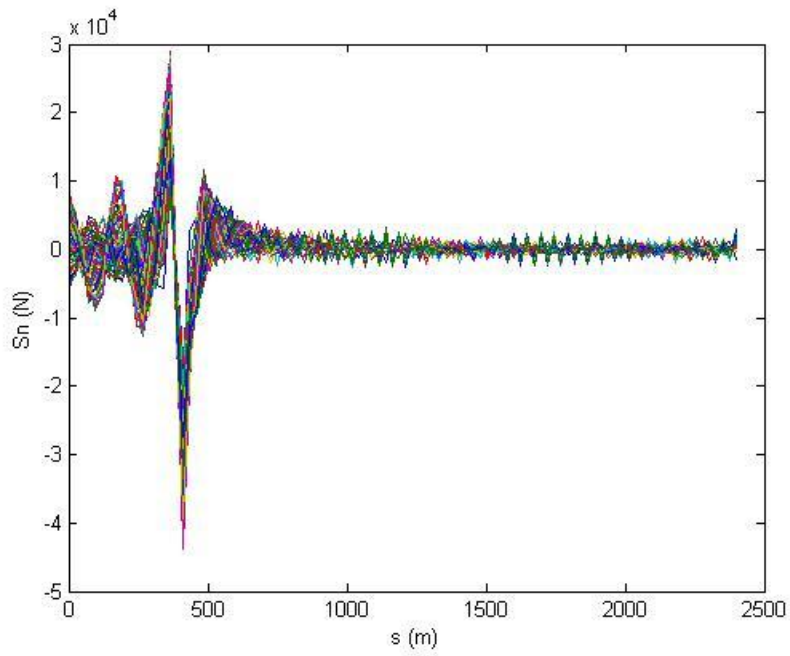
5.1.2.  $m$   $S_n$   $1 \text{ rad/s.}$   $1$   
 -  $\text{TDP } 2515 \text{ N/m}$



5.1.2.  $3$   $1 \text{ rad/s.}$   $1 \text{ m}$   
 -  $\text{TDP } 2515 \text{ N/m}$

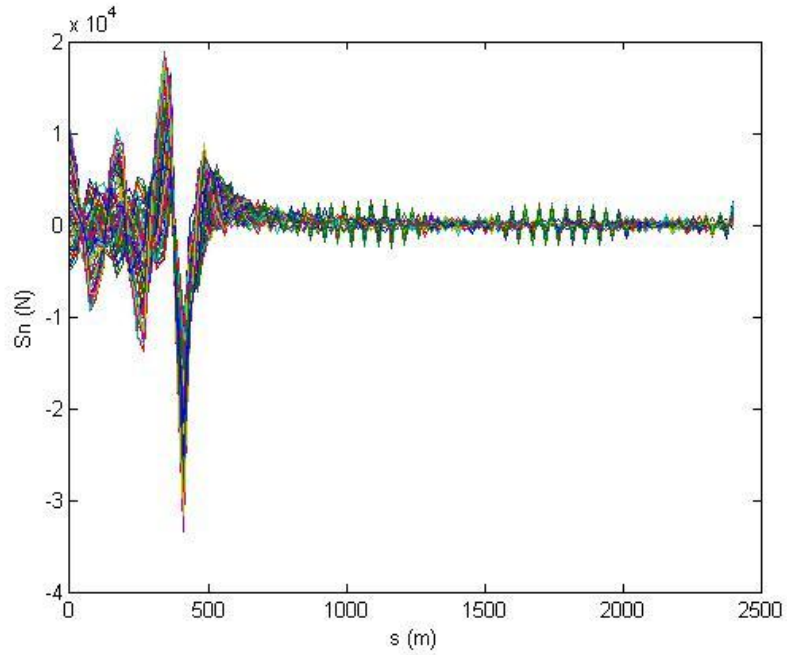


5.1.1.3.  $T$  1 rad/s. 1 m  
 - TDP 4226 N/m

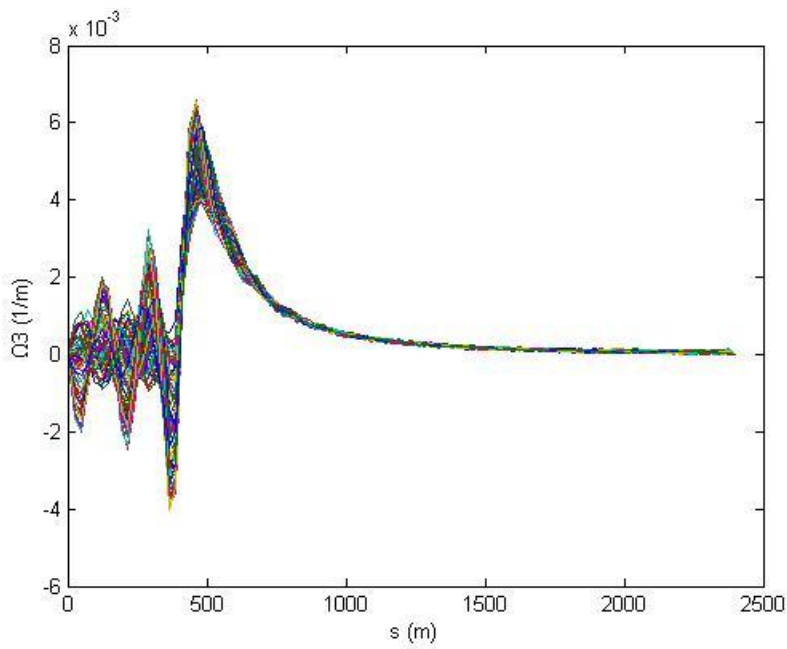


5.1.1.3.  $S_n$  1 rad/s. 1 m  
 m - TDP 4226 N/m



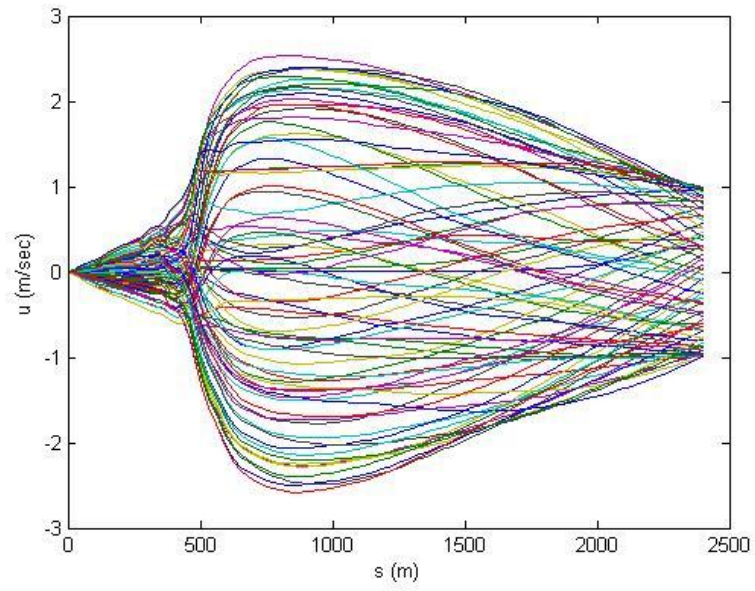


5.1.4.  $m$   $S_n$   $1 \text{ rad/s.}$   $1$   
 -  $\text{TDP } 2696 \text{ N/m}$

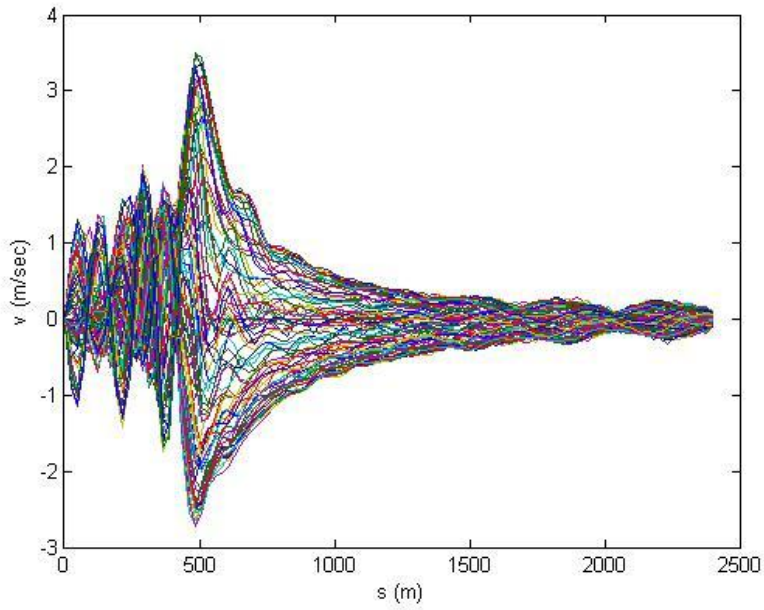


5.1.4.  $3$   $1 \text{ rad/s.}$   $1 \text{ m}$   
 -  $\text{TDP } 2696 \text{ N/m}$   
 5.1.5 - 5.1.8:

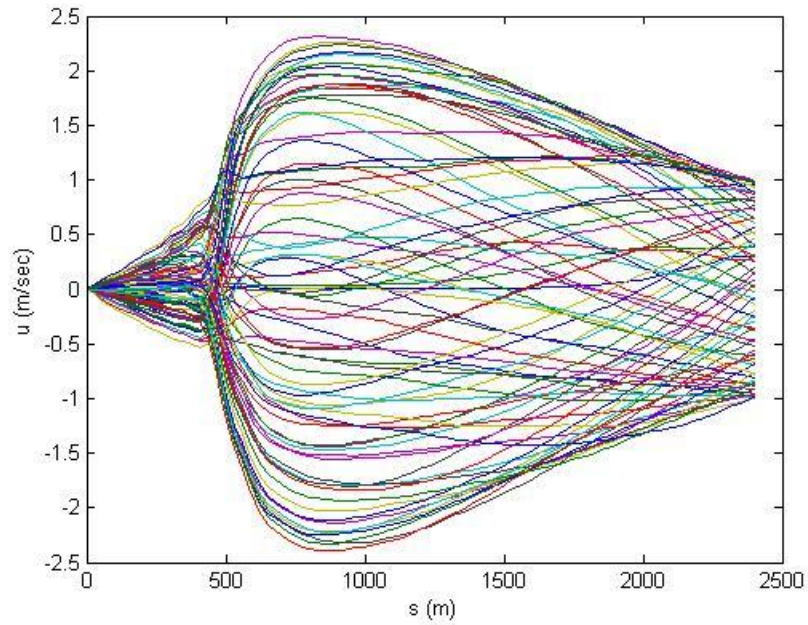
,  $s$ ,  
 heave 1 m:



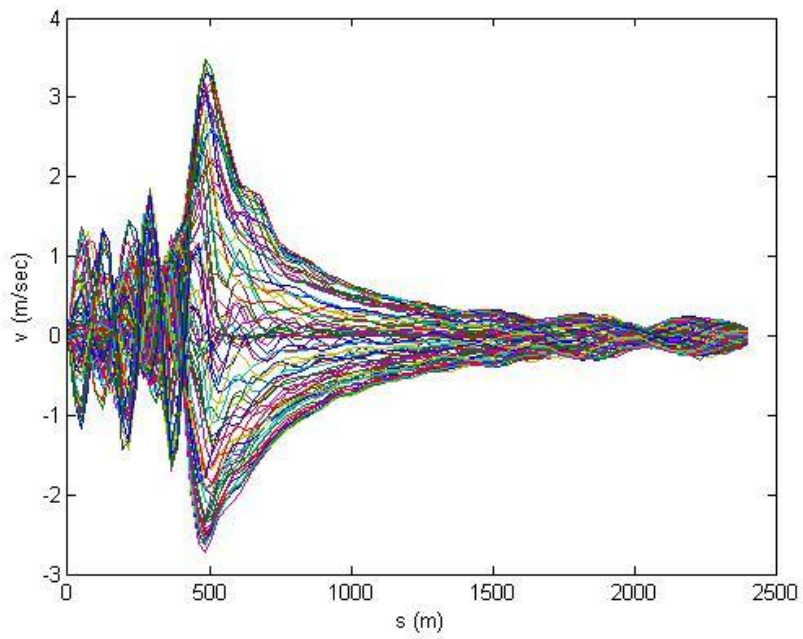
5.1.5. 1 m,  $u$ , 1 rad/s.  
 - TDP 3575 N/m



5.1.5. 1 m,  $v$ , 1 rad/s.  
 - TDP 3575 N/m

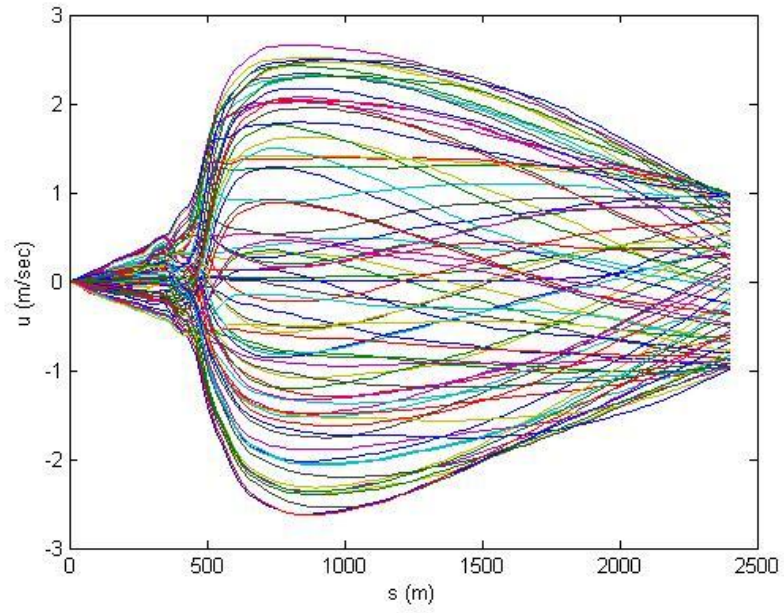


5.1.6.  $u$ ,  $1 \text{ m}$ ,  $1 \text{ rad/s}$ ,  $\text{TDP } 2515 \text{ N/m}$

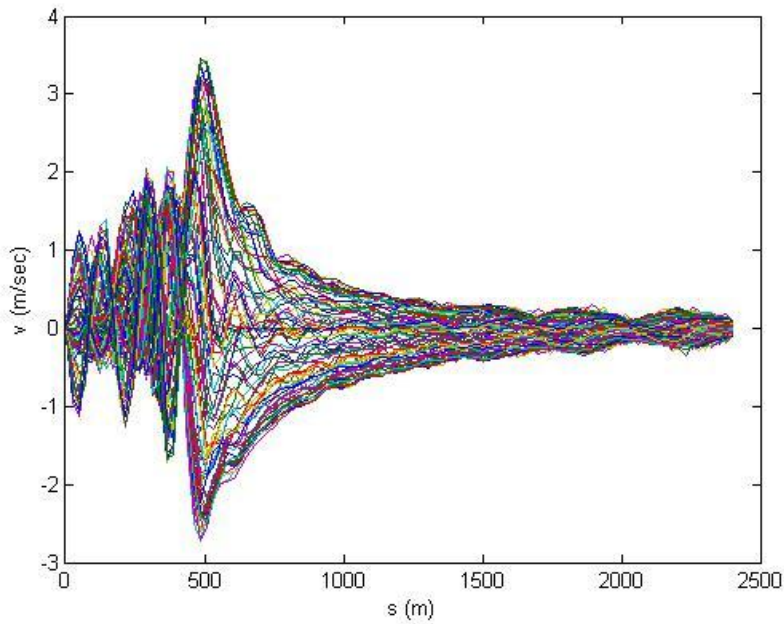


5.1.6.  $v$ ,  $1 \text{ m}$ ,  $1 \text{ rad/s}$ ,  $\text{TDP } 2515 \text{ N/m}$

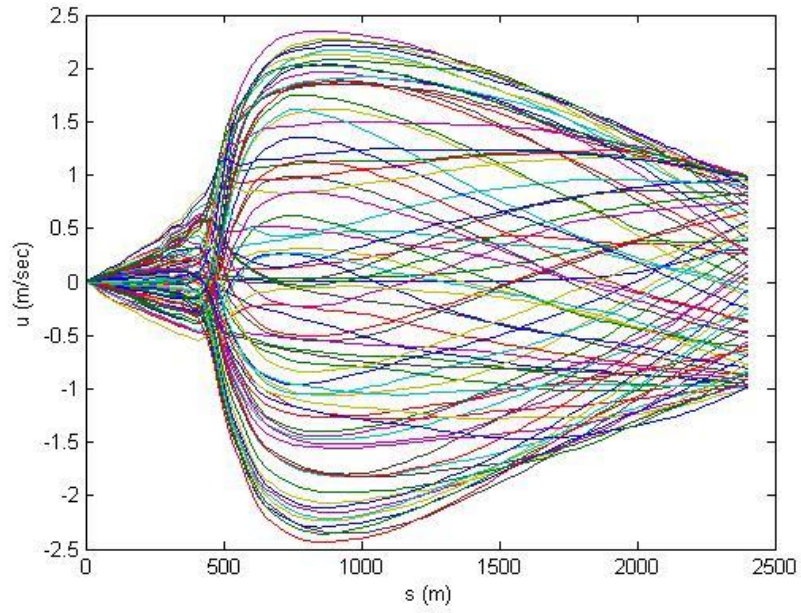




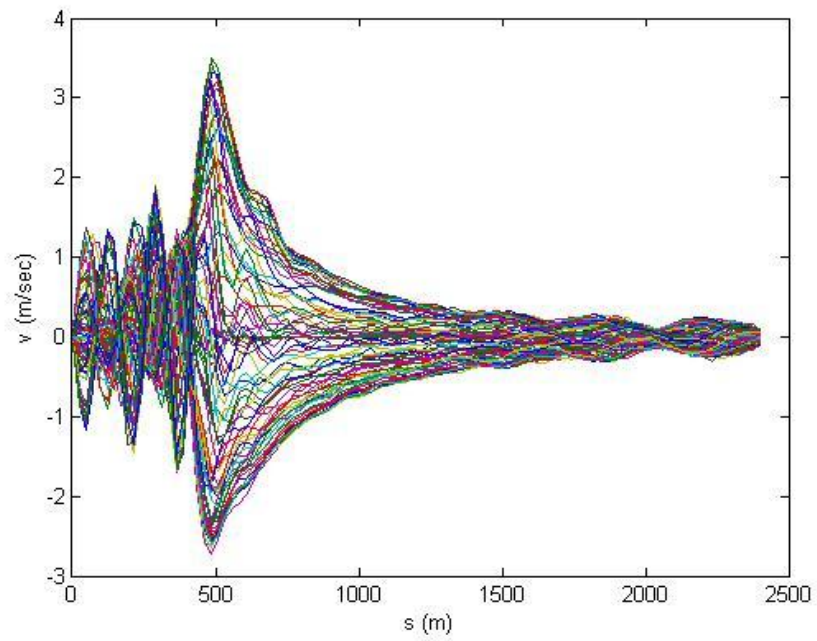
5.1.7.  $\omega = 1 \text{ rad/s}$ ,  $\tau = 1 \text{ m}$ ,  $TDP = 4226 \text{ N/m}$



5.1.7.  $\omega = 1 \text{ rad/s}$ ,  $\tau = 1 \text{ m}$ ,  $TDP = 4226 \text{ N/m}$



5.1.8.  $\omega = 1 \text{ rad/s}$ ,  $\text{TDP} = 2696 \text{ N/m}$

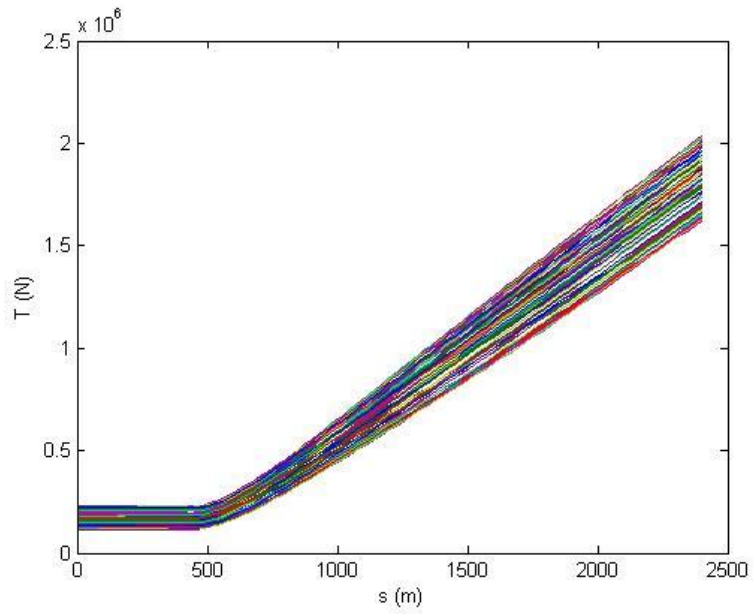


5.1.8.  $\omega = 1 \text{ rad/s}$ ,  $\text{TDP} = 2696 \text{ N/m}$

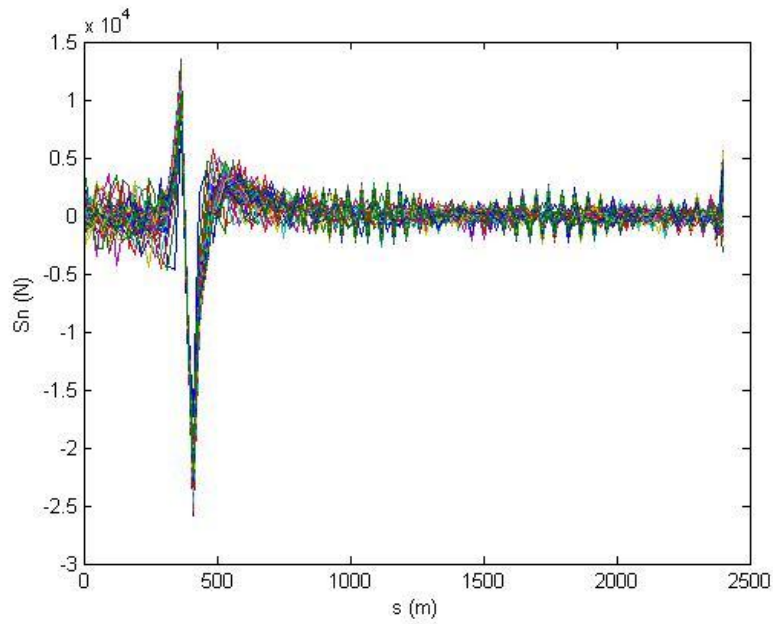


5.1.9 - 5.1.12:

, s, \_\_\_\_\_  
 \_\_\_\_\_ surge 1 m

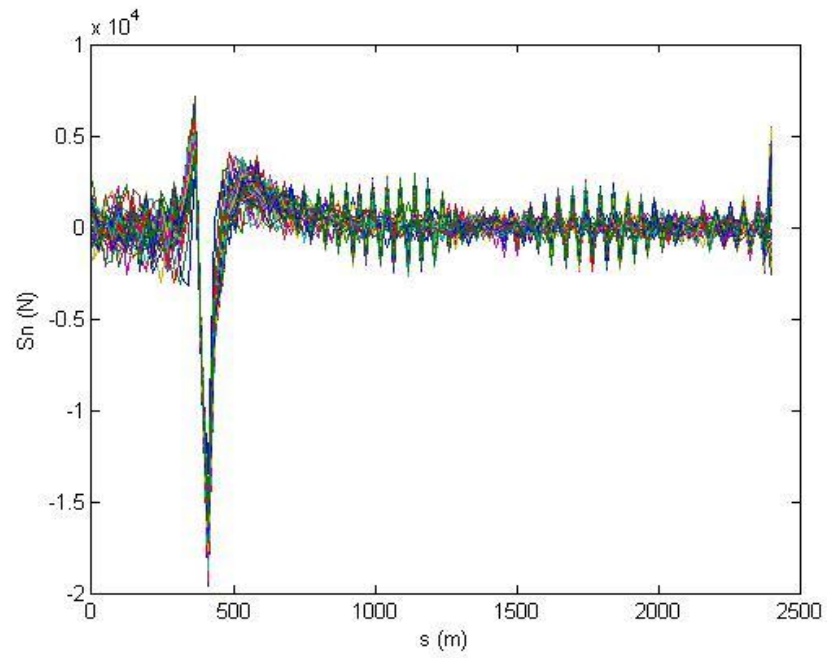


5.1.9.  $T$  1 m  
 1 rad/s.  
 TDP 3575 N/m

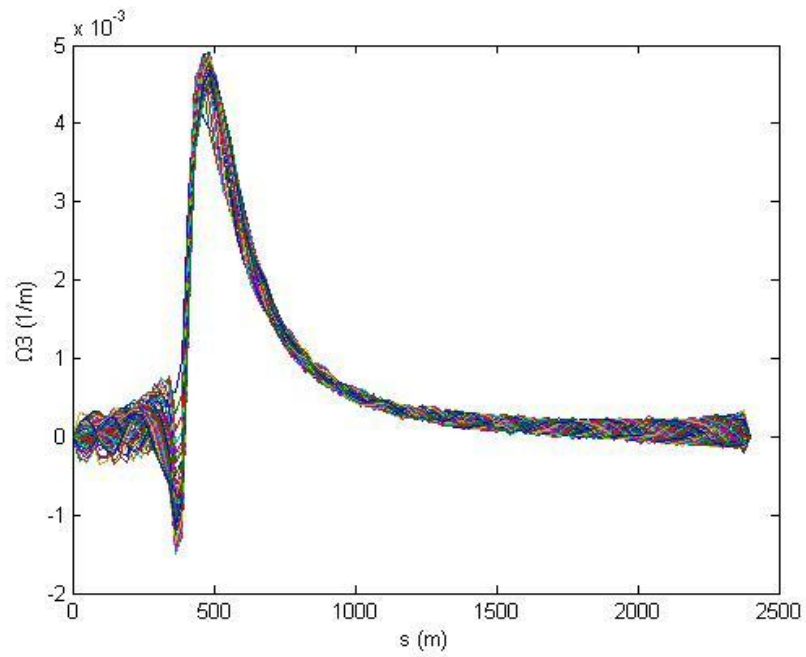


5.1.9.  $S_n$  1 m  
 1 rad/s.  
 TDP 3575 N/m

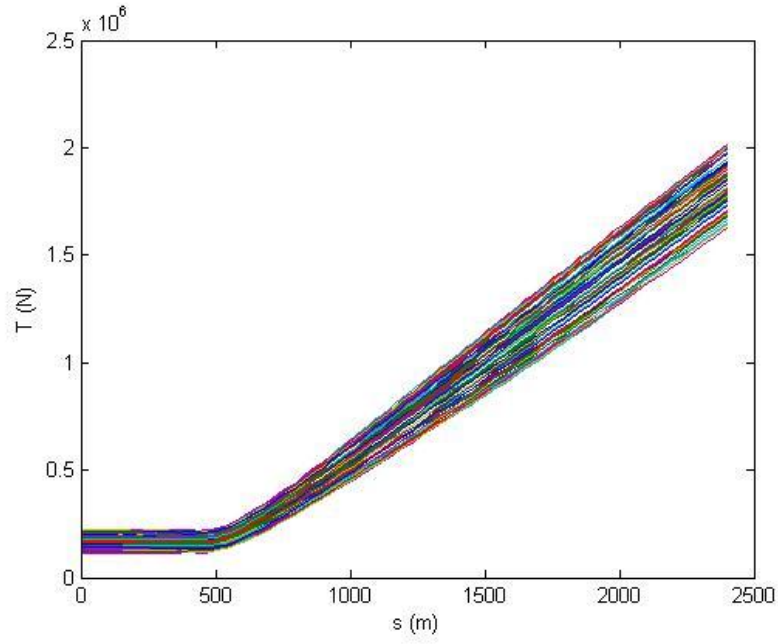




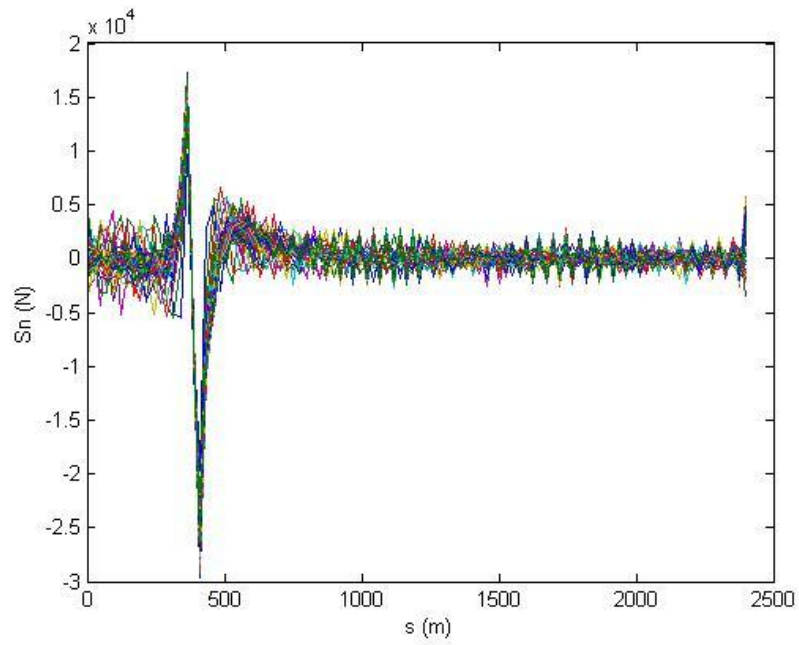
5.1.10. Sn 1 rad/s. 1 m  
 - TDP 2515 N/m



5.1.10. 3 1 rad/s. 1 m  
 - TDP 2515 N/m

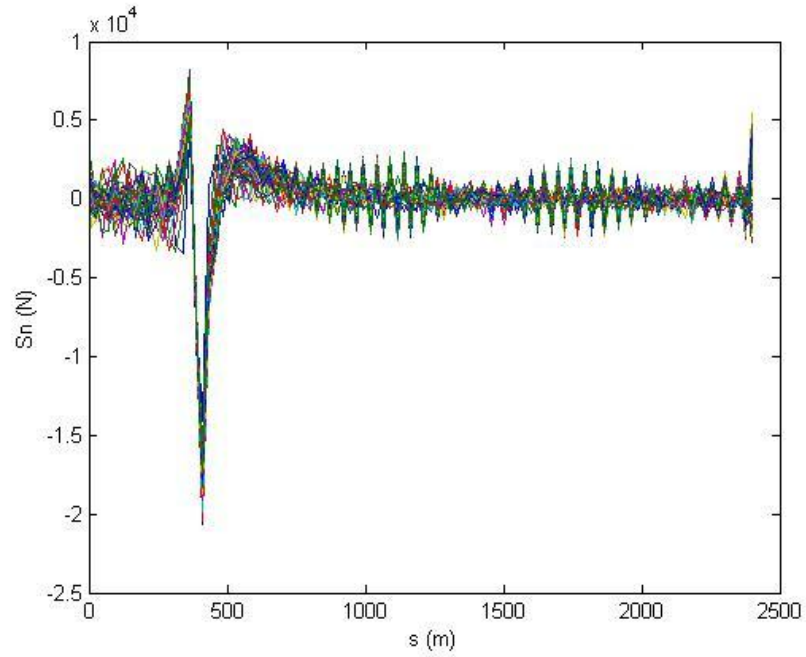


5.1.11.  $T$  1 rad/s. 1 m  
 - TDP 4226 N/m

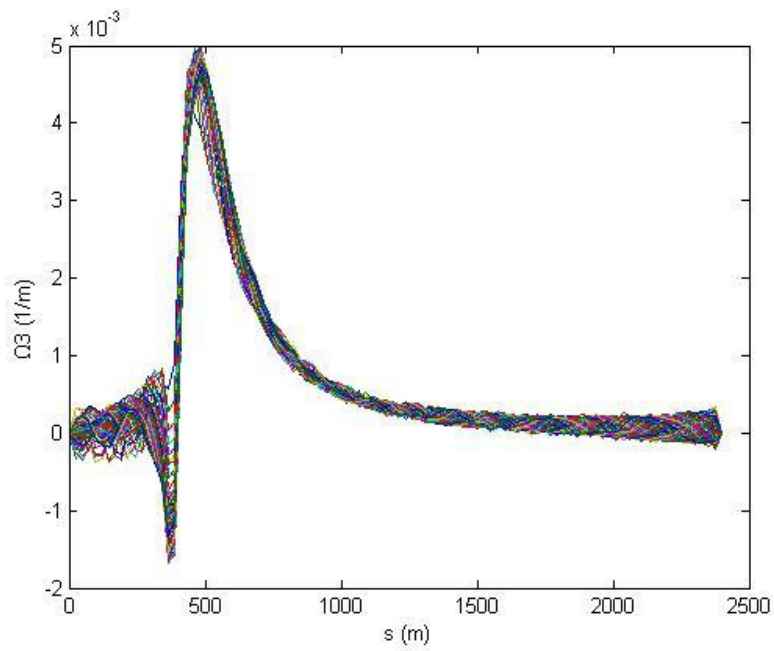


5.1.11.  $S_n$  1 rad/s. 1 m  
 - TDP 4226 N/m





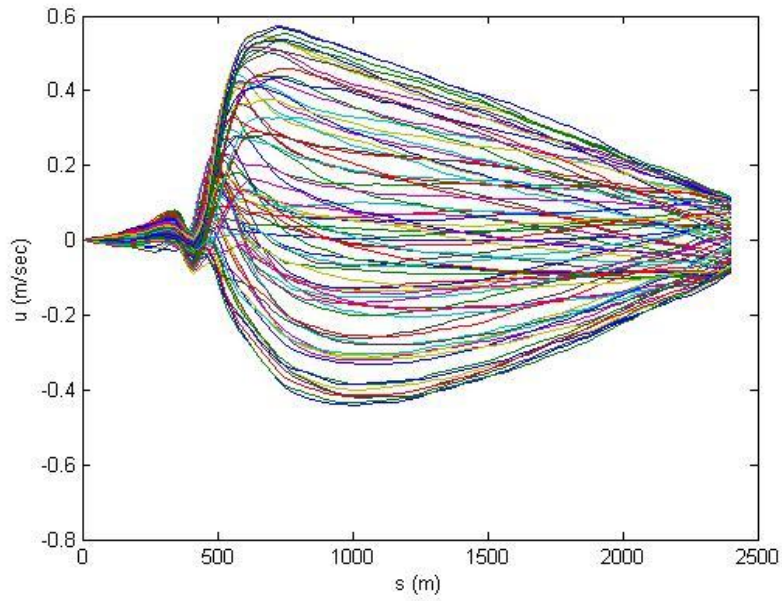
5.1.12.  $S_n$  1 rad/s. 1 m  
 - TDP 2696 N/m



5.1.12. 3 1 rad/s. 1 m  
 - TDP 2696 N/m

5.1.13 - 5.1.16:

surge 1 m:



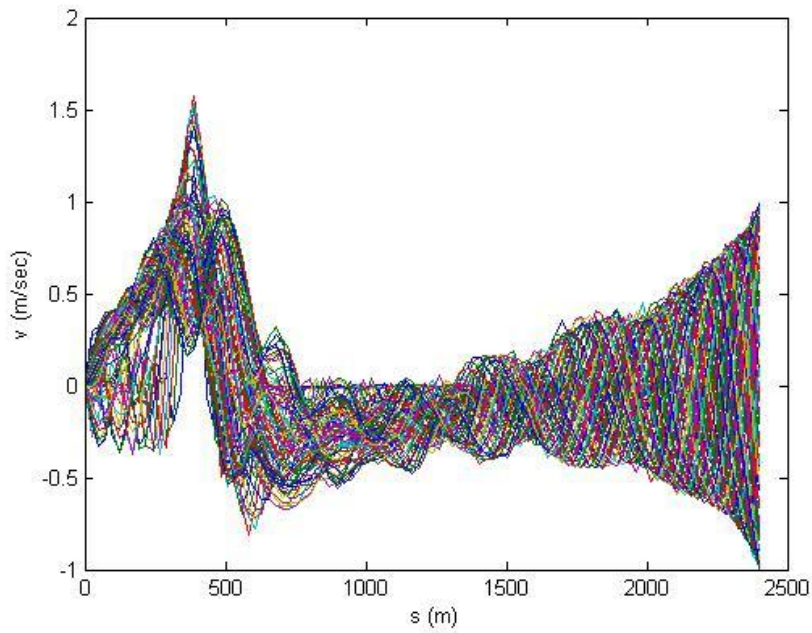
5.1.13.

1 m

, u,

1rad/s.

TDP 3575 N/m



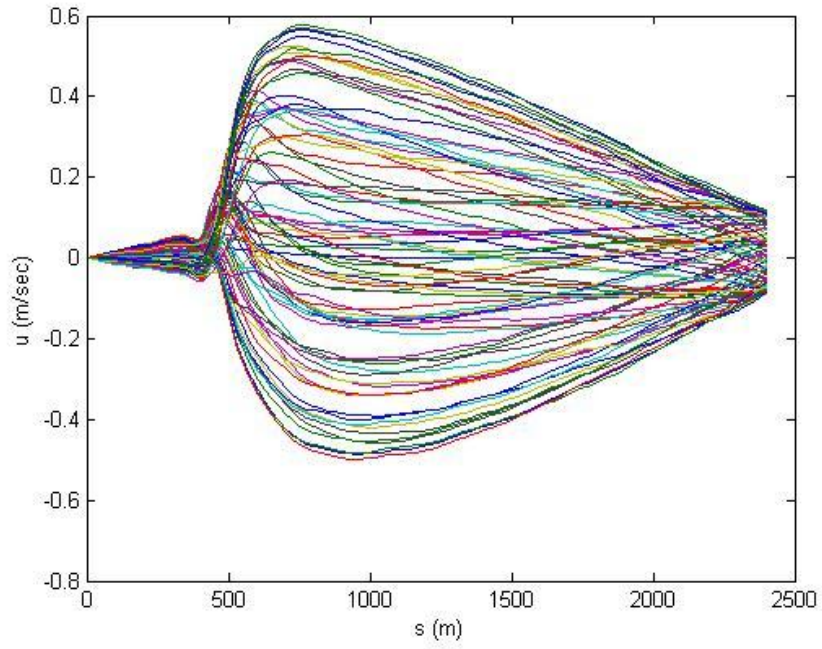
5.1.13.

1 m

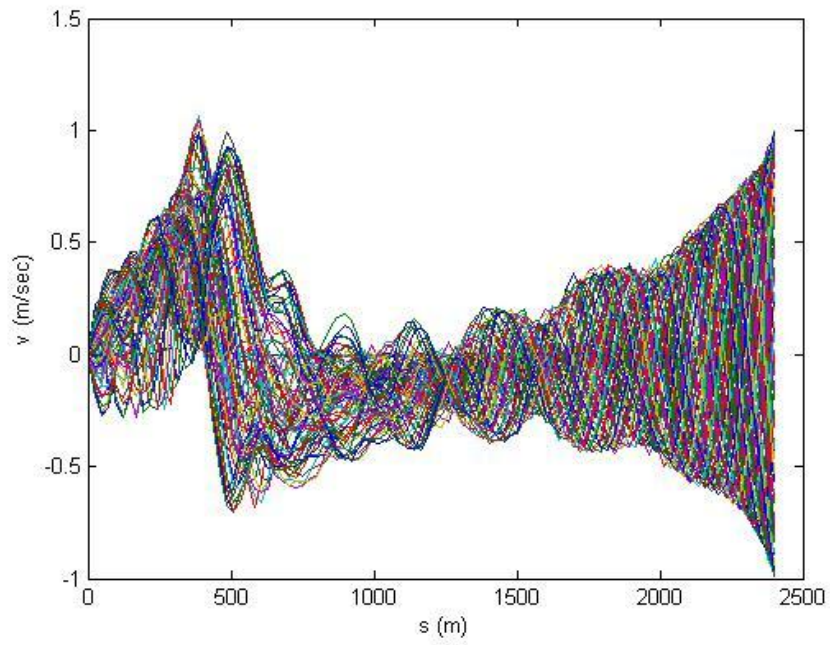
, v,

1rad/s.

TDP 3575 N/m

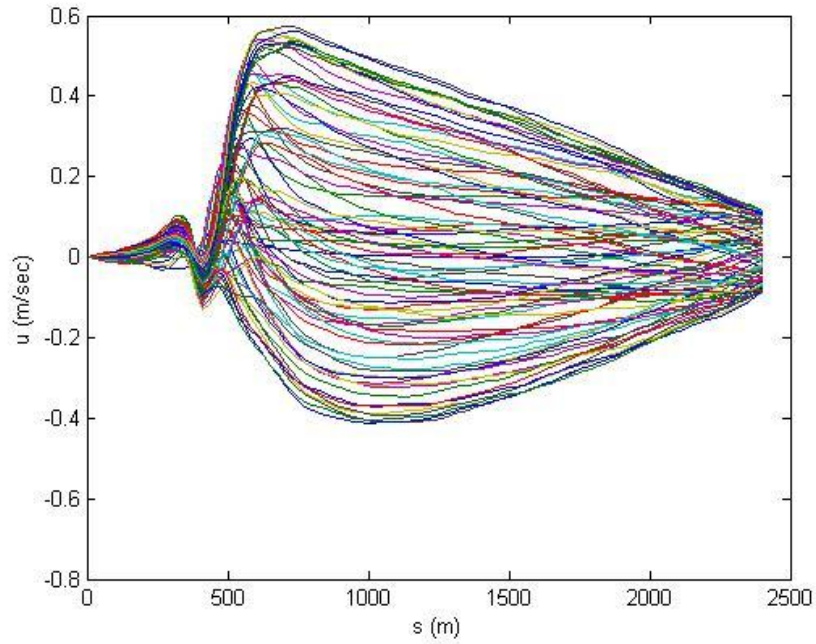


5.1.14.  $1 \text{ m}$ ,  $u$ ,  $1 \text{ rad/s}$ .  
 - TDP 2515 N/m

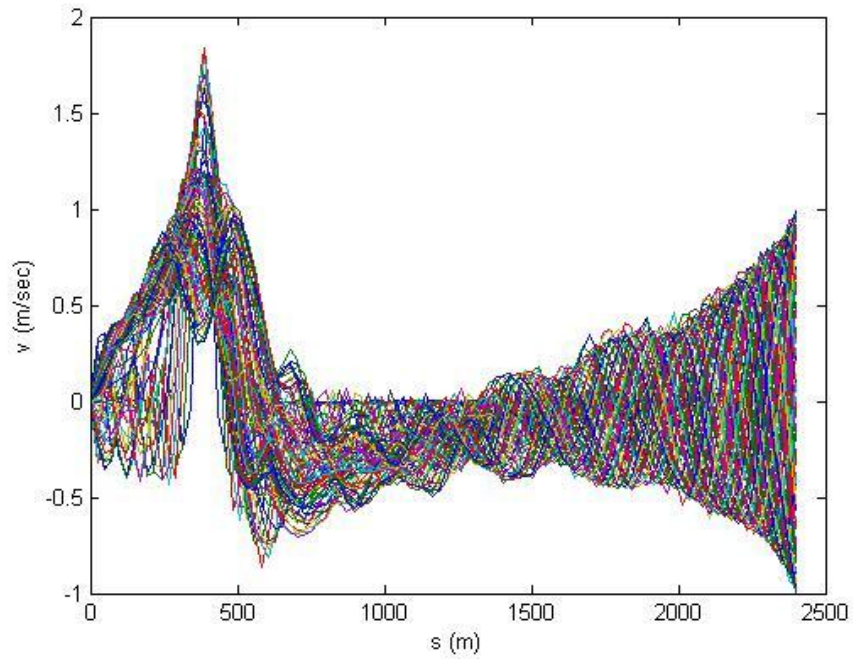


5.1.14.  $1 \text{ m}$ ,  $v$ ,  $1 \text{ rad/s}$ .  
 - TDP 2515 N/m

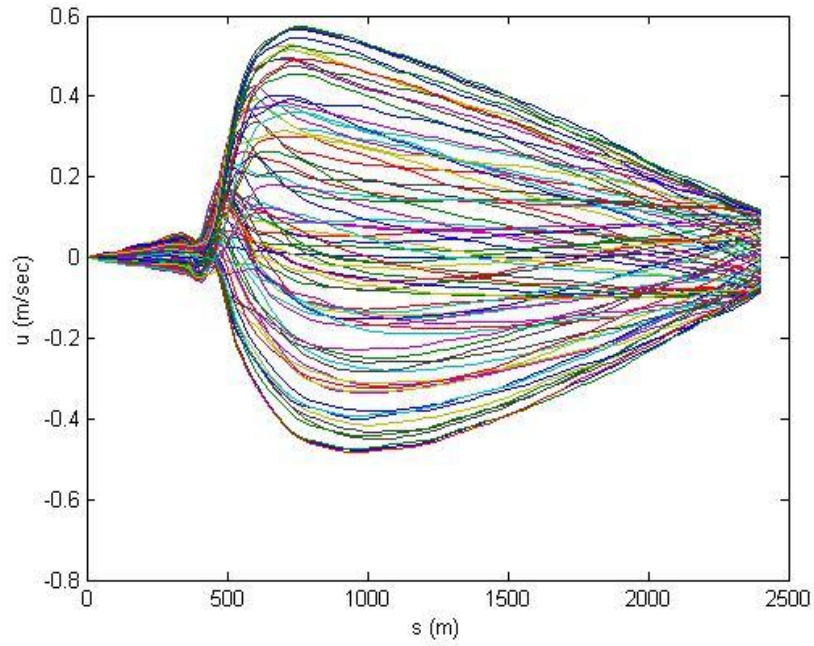




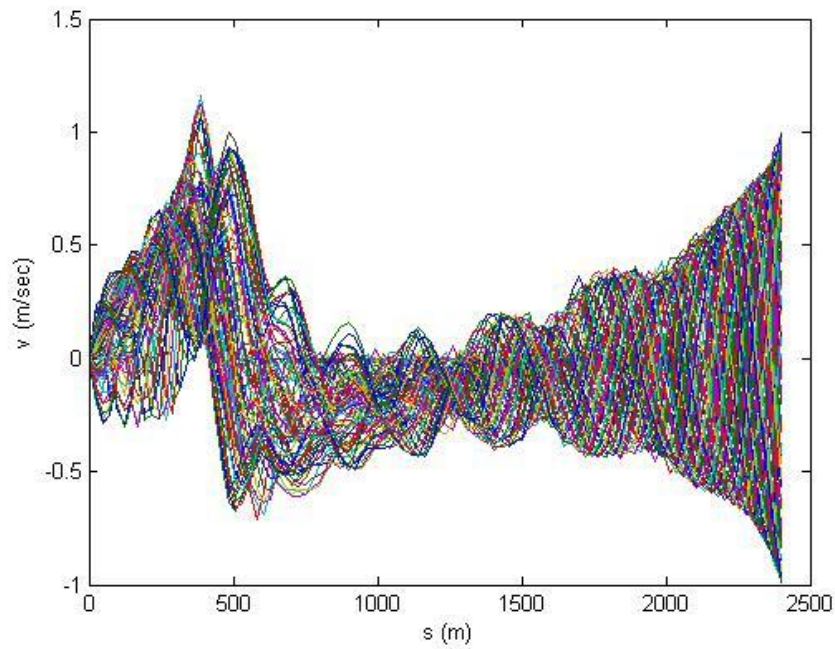
5.1.15. 1 m, u, 1rad/s.  
- TDP 4226 N/m



5.1.15. 1 m, v, 1rad/s.  
- TDP 4226 N/m



5.1.16.  $1 \text{ m}$ ,  $u$ ,  $1 \text{ rad/s}$ ,  
 $-$  TDP 2696 N/m



5.1.16.  $1 \text{ m}$ ,  $v$ ,  $1 \text{ rad/s}$ ,  
 $-$  TDP 2696 N/m

s 0 400 m, riser, x y.

• (surge) heave 3 ( 3= 3).

• riser ( 1/2 ).

surge : E , 3, 0 /

riser , Sn ( x-z)

Sn TDP.

-heave

:

•

,

.

/

(buckling) TDP, ' ,

•

TDP , ,

•

(

riser

,

)

•

TDP.

,

/

riser.

•

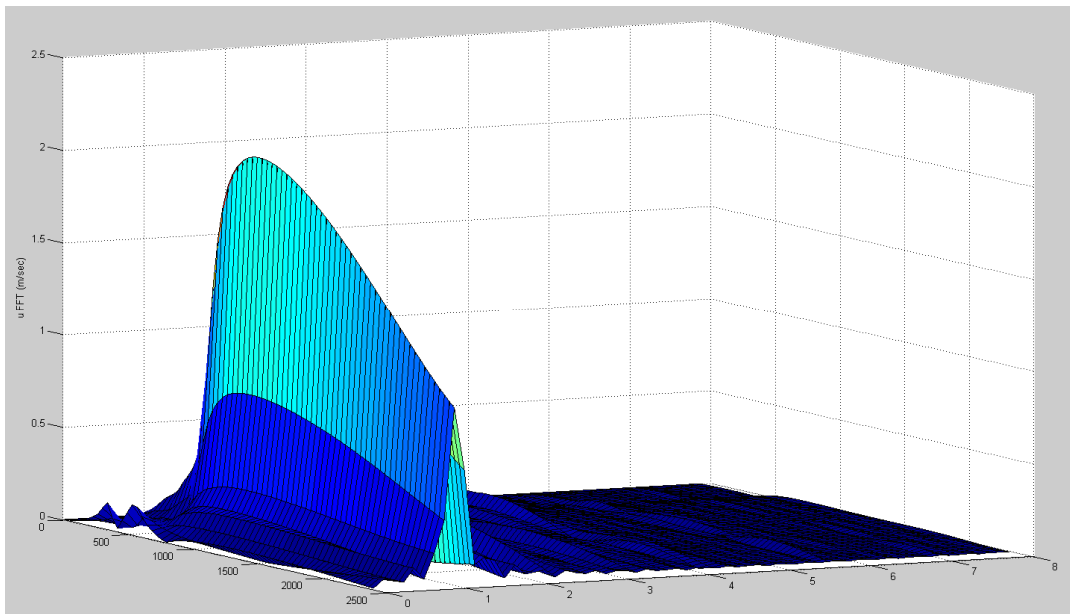
,

,

TDP

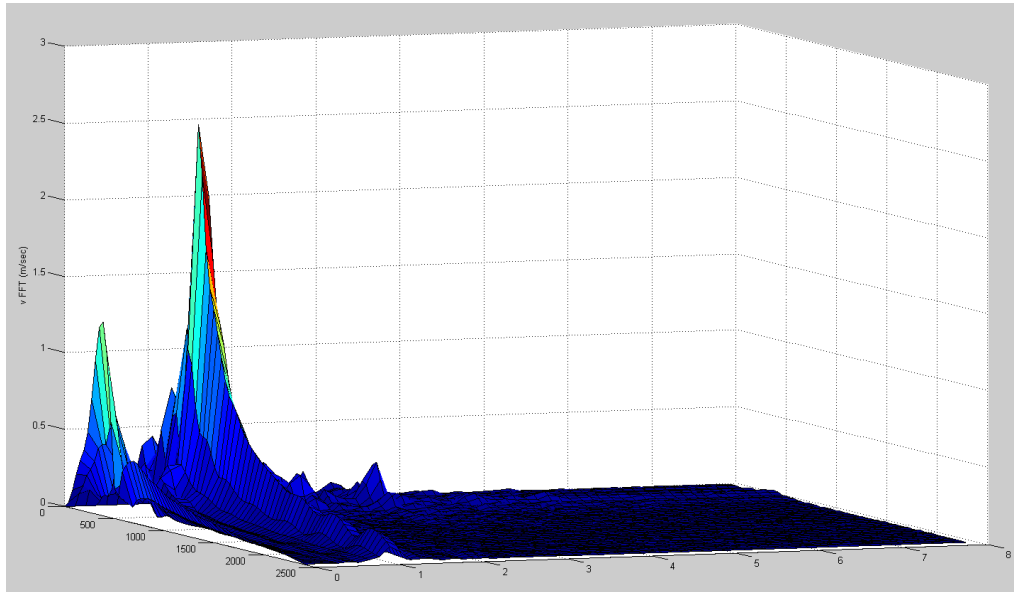
5.3

(time-domain)  
CON3DF, (frequency-domain).  
(FFT), Matlab Fourier  
z=1 m, 1 rad/sec,  
riser 2.5D, 2R/3  
5  
(n=400)



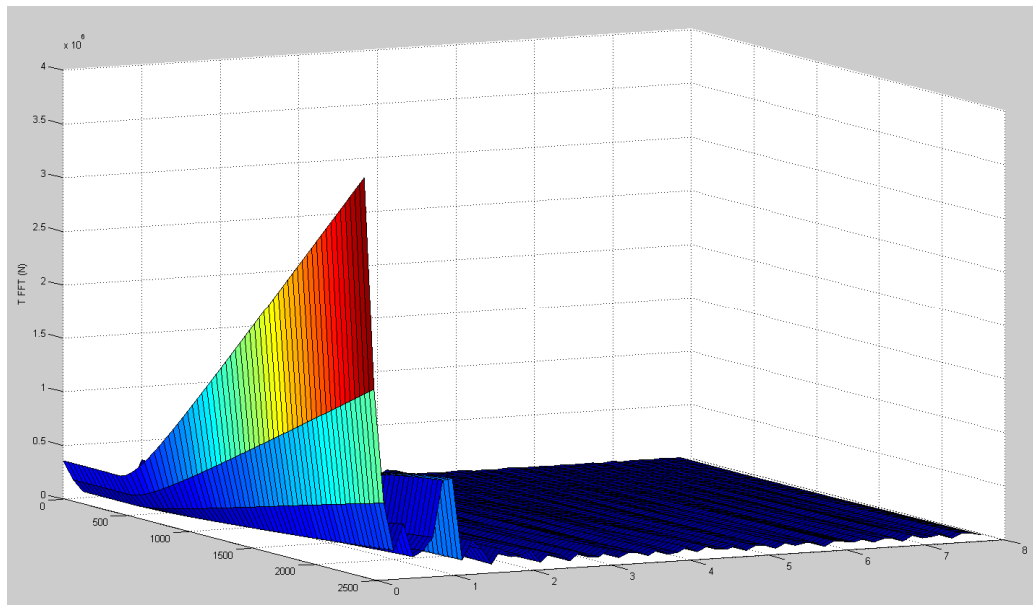
5.2.1.

1 m 1 rad/sec.  
TDP 4226N/m



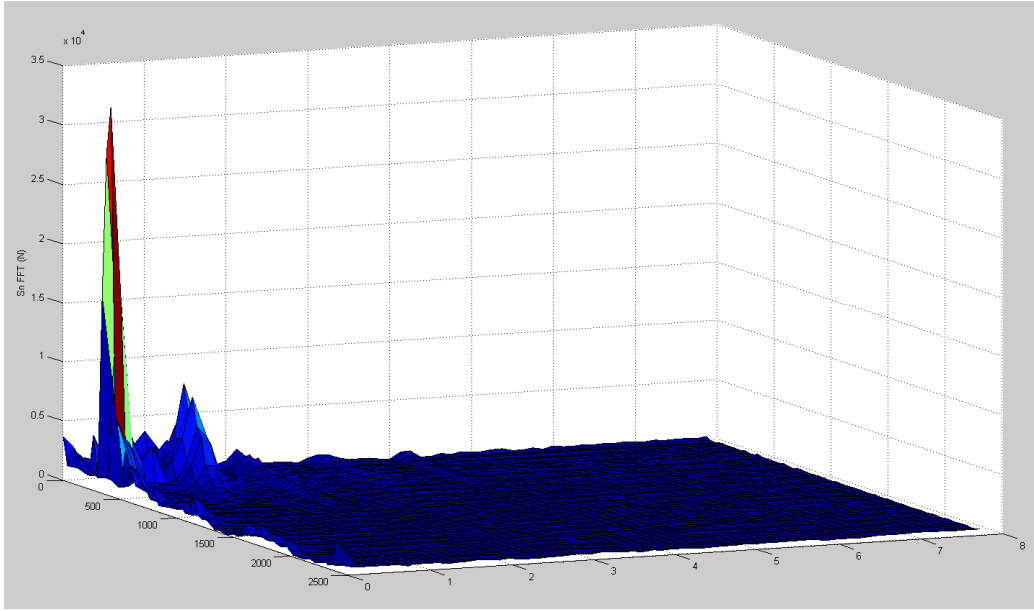
5.2.2.

1 m            1 rad/sec.  
TDP 4226N/m



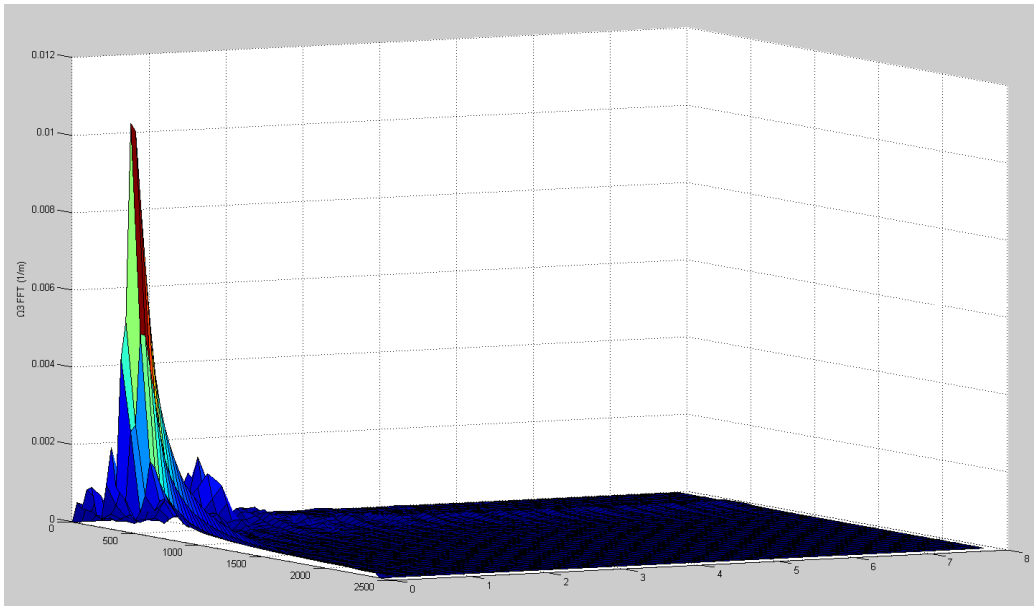
5.2.3.

1 m            1 rad/sec.  
TDP 4226N/m



5.2.4.

1 m      1 rad/sec.  
TDP 4226N/m



5.2.5.

1 m      1 rad/sec.  
TDP 4226N/m

1000m

3

( )

TDP.





6. -

6.1

3 5,

:

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riser ,

riser- .

•

, 15 kN/m 5

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riser- .

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riser

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TDP,

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"sagbend",

TDP

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• , ,  
TDP . ,

, 9

"CON3DF".

• ,  
• ,  
• ,

( dm).

## 6.2

,  
riser/

(Ultra Deep Sonars  
Autonomous Underwater Vehicles/AUV), 20 cm<sup>2</sup>  
, 2000 m .

,  
dm. ,



32 33] riser (CFD), "Fluid - Structure Interaction". risers, (Multi-Phase flow), TDP, [3, 9,

[47],

" [1, 3].

CON3DF,

Bernoulli (

)



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- RISER TDP ,  
PHASE 2

.1. -

.1.1.

1/3 D

A .	0.1 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0

A .	0.5 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	7	0
5	7	0
6	7	0
7	7	0
8	0	0
9	0	0
10	0	0

A .	D	
	xx (kPa)	yy (kPa)
1	9	0
2	9	0
3	9	0
4	9	0
5	9	0
6	9	0
7	9	0
8	9	0
9	9	0
10	9	0

A .	1.5 D	
	xx (kPa)	yy (kPa)
1	14	6.5
2	14	6.5
3	14	6.5
4	21	0
5	21	0
6	21	0
7	21	0
8	14	6.5
9	14	6.5
10	14	6.5

A .	2 D	
	xx (kPa)	yy (kPa)
1	14	6.5
2	21	6.5
3	28	6.5
4	28	6.5
5	35	6.5
6	35	6.5
7	28	6.5
8	28	6.5
9	21	6.5
10	14	6.5

A .		2.5 D
	xx (kPa)	yy (kPa)
1	23,5	6.5
2	31	6.5
3	38.5	6.5
4	38.5	6.5
5	46	6.5
6	46	6.5
7	38.5	6.5
8	38.5	6.5
9	31	6.5
10	23.5	6.5

A .		3 D
	xx (kPa)	yy (kPa)
1	31	12
2	38.5	12
3	46	12
4	53.5	6
5	53.5	6
6	53.5	6
7	53.5	6
8	46	12
9	38.5	12
10	31	12

A .		3.5 D
	xx (kPa)	yy (kPa)
1	38.5	12
2	53.5	12
3	68.5	12
4	68.5	6
5	76	6
6	76	12
7	68.5	12
8	68.5	12
9	61	12
10	46	12



A .		4 D
	xx (kPa)	yy (kPa)
1	45.5	18
2	52	18
3	71,5	12
4	84,5	12
5	84,5	12
6	97.5	6
7	84.5	12
8	78	12
9	65	18
10	52	18

A .		4.5 D
	xx (kPa)	yy (kPa)
1	65	18
2	78	18
3	84,5	18
4	91	12
5	97.5	12
6	104	12
7	104	12
8	97,5	18
9	84,5	18
10	71.6	18

A .		5 D
	xx (kPa)	yy (kPa)
1	64	18
2	71	18
3	92	18
4	99	12
5	113	18
6	113	18
7	106	12
8	106	18
9	85	18
10	64	18

A .	0.1 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0

A .	0.5 D	
	xx (kPa)	yy (kPa)
1	1	0
2	1	0
3	1	0
4	1	0
5	1	0
6	1	0
7	1	0
8	1	0
9	1	0
10	1	0

A .	D	
	xx (kPa)	yy (kPa)
1	1	6.5
2	9	6.5
3	9	6.5
4	9	0
5	9	0
6	9	0
7	9	6.5
8	9	6.5
9	9	6.5
10	1	6.5

A .	1.5 D	
	xx (kPa)	yy (kPa)
1	9	13
2	9	6.5
3	17	6.5
4	17	6.5
5	25	0
6	25	0
7	17	0
8	17	6.5
9	9	6.5
10	9	13

A .	2 D	
	xx (kPa)	yy (kPa)
1	9	13
2	17	13
3	25	13
4	28	6.5
5	33	6.5
6	33	6.5
7	33	13
8	25	13
9	17	13
10	9	13

A .	2.5 D	
	xx (kPa)	yy (kPa)
1	21	19.5
2	28	19.5
3	35	13
4	42	13
5	49	6.5
6	49	6.5
7	42	13
8	35	13
9	28	19.5
10	21	19.5

A .		3 D
	xx (kPa)	yy (kPa)
1	23.5	21
2	31	21
3	38.5	21
4	46	14
5	61	14
6	53.5	14
7	53.5	14
8	46	21
9	38.5	21
10	31	21

A .		3.5 D
	xx (kPa)	yy (kPa)
1	35	24
2	35	24
3	49	18
4	49	18
5	63	12
6	70	12
7	70	18
8	63	18
9	49	24
10	35	24

A .		4 D
	xx (kPa)	yy (kPa)
1	52	26
2	65	26
3	78	19.5
4	91	19.5
5	97.5	12
6	97.5	12
7	84.5	19.5
8	84.5	19.5
9	78	26
10	65	32.5

A .	4.5 D	
	xx (kPa)	yy (kPa)
1	65	36
2	71.5	30
3	78	24
4	104	12
5	97.5	12
6	104	24
7	97.5	24
8	84.5	30
9	78	30
10	65	36

A .	5 D	
	xx (kPa)	yy (kPa)
1	58.5	36
2	91	36
3	97.5	36
4	110.5	30
5	123.5	24
6	117	12
7	97.5	18
8	84.5	30
9	84.5	36
10	58.5	36

.1.3.

D

A .	0.1 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0

A .	0.5 D	
	xx (kPa)	yy (kPa)
1	1	0
2	1	0
3	1	0
4	1	0
5	1	0
6	1	0
7	1	0
8	1	0
9	1	0
10	1	0

A .	D	
	xx (kPa)	yy (kPa)
1	1	6.5
2	1	6.5
3	1	6.5
4	9	6.5
5	9	0
6	17	0
7	9	6.5
8	9	6.5
9	1	6.5
10	1	6.5

A .	1.5 D	
	xx (kPa)	yy (kPa)
1	1	6.5
2	1	13
3	9	13
4	17	6.5
5	17	6.5
6	25	6.5
7	17	6.5
8	17	13
9	9	13
10	1	6.5

A .	2 D	
	xx (kPa)	yy (kPa)
1	9	19.5
2	9	19.5
3	17	13
4	25	13
5	33	6.5
6	33	6.5
7	25	13
8	25	13
9	17	19.5
10	9	19.5

A .	2.5 D	
	xx (kPa)	yy (kPa)
1	21	26
2	28	26
3	35	19.5
4	42	13
5	49	6.5
6	49	6.5
7	42	13
8	35	19.5
9	28	26
10	21	26

A .	3 D	
	xx (kPa)	yy (kPa)
1	21	32.5
2	28	26
3	42	19.5
4	56	13
5	56	13
6	56	13
7	56	19.5
8	42	26
9	28	26
10	21	32.5

A .		3.5 D
	xx (kPa)	yy (kPa)
1	28	39
2	35	32.5
3	49	26
4	70	19.5
5	77	13
6	77	13
7	70	19,5
8	49	26
9	42	32.5
10	28	39

A .		4 D
	xx (kPa)	yy (kPa)
1	28	45.5
2	35	45.5
3	63	32.5
4	84	26
5	105	19,5
6	91	19.5
7	84	26
8	56	32.5
9	42	45.5
10	28	45.5

A .		4.5 D
	xx (kPa)	yy (kPa)
1	58	48
2	66	42
3	82	30
4	98	24
5	98	24
6	98	24
7	70	36
8	50	42
9	42	48
10	34	60



A .	5 D	
	xx (kPa)	yy (kPa)
1	74	45,5
2	82	39
3	98	32,5
4	114	32,5
5	114	32,5
6	114	32,5
7	106	32,5
8	98	39
9	82	45,5
10	58	58,5

.2. -

.2.1.

1/3 D

A .	0.1 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0

A .	0.5 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	0	0
5	7	0
6	7	0
7	0	0
8	0	0
9	0	0
10	0	0

A .	D	
	xx (kPa)	yy (kPa)
1	8.5	0
2	8.5	0
3	8.5	0
4	8.5	0
5	8.5	0
6	8.5	0
7	8.5	0
8	8.5	0
9	8.5	0
10	8.5	0

A .	1.5 D	
	xx (kPa)	yy (kPa)
1	8.5	5.5
2	8.5	5.5
3	16	5.5
4	16	5.5
5	23.5	0
6	23.5	0
7	16	5.5
8	16	5.5
9	8.5	5.5
10	8.5	5.5

A .	2 D	
	xx (kPa)	yy (kPa)
1	13	5.5
2	19.5	5.5
3	26	5.5
4	26	5.5
5	32.5	5.5
6	32.5	5.5
7	26	5.5
8	26	5.5
9	19.5	5.5
10	19.5	5.5

A .		2.5 D
	xx (kPa)	yy (kPa)
1	32.5	11
2	32.5	5.5
3	39	5.5
4	39	5.5
5	45.5	5.5
6	39	5.5
7	39	5.5
8	39	5.5
9	26	5.5
10	19.5	11

A .		3 D
	xx (kPa)	yy (kPa)
1	32.5	11
2	39	11
3	45.5	11
4	58.5	5.5
5	52	5.5
6	52	5.5
7	52	5.5
8	45.5	11
9	39	11
10	32.5	11

A .		3.5 D
	xx (kPa)	yy (kPa)
1	43	11
2	50	11
3	57.5	11
4	71	5.5
5	71	5.5
6	64	11
7	64	11
8	64	11
9	50	11
10	43	11

A .		4 D
	xx (kPa)	yy (kPa)
1	50	16.5
2	50	<b>16.5</b>
3	71	11
4	85	11
5	78	11
6	92	5.5
7	78	11
8	71	11
9	64	16.5
10	57	16.5

A .		4.5 D
	xx (kPa)	yy (kPa)
1	64	16.5
2	78	16.5
3	85	16.5
4	99	11
5	99	11
6	99	11
7	99	11
8	78	16.5
9	64	16.5
10	57	16.5

A .		5 D
	xx (kPa)	yy (kPa)
1	66	16.5
2	72	16.5
3	84	16.5
4	96	16.5
5	108	16.5
6	108	16.5
7	102	16.5
8	102	16.5
9	78	16.5
10	66	16.5

.2.2.

2/3 D

A .	0.1 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0

A .	0.5 D	
	xx (kPa)	yy (kPa)
1	1	0
2	1	0
3	1	0
4	1.05	0
5	1.05	0
6	1.05	0
7	1.05	0
8	1 0	0
9	1 0	0
10	1 0	0

A .	D	
	xx (kPa)	yy (kPa)
1	1	5.5
2	8.5	5.5
3	8.5	5.5
4	8.5	0
5	8.5	0
6	8.5	0
7	8.5	0
8	8.5	5.5
9	8.5	5.5
10	1	5.5

A .		1.5 D
	xx (kPa)	yy (kPa)
1	8.5	6
2	16	6
3	16	6
4	23.5	0
5	23.5	0
6	23.5	0
7	16	6
8	16	6
9	8.5	6
10	8.5	6

A .		2 D
	xx (kPa)	yy (kPa)
1	16	13
2	16	13
3	23.5	13
4	31	6.5
5	31	6.5
6	31	6.5
7	31	6.5
8	23.5	6.5
9	16	13
10	16	13

A .		2.5 D
	xx (kPa)	yy (kPa)
1	16	16.5
2	31	16.5
3	31	11
4	38.5	11
5	46	5.5
6	46	5.5
7	38.5	11
8	31	11
9	31	16.5
10	23.5	16.5

A .	3 D	
	xx (kPa)	yy (kPa)
1	31	21
2	38.5	21
3	38.5	14
4	53.5	14
5	61	14
6	53.5	14
7	53.5	14
8	46	14
9	38.5	21
10	23.5	21

A .	3.5 D	
	xx (kPa)	yy (kPa)
1	43	11
2	57.5	11
3	71	13
4	71	5.5
5	71	11
6	64	11
7	64	11
8	64	11
9	50	16.5
10	43	11

A .	4 D	
	xx (kPa)	yy (kPa)
1	39	27.5
2	52	27.5
3	71.5	22
4	71.5	16.5
5	91	11
6	84.5	11
7	78	11
8	71.5	22
9	52	22
10	39	27.5

A .		4.5 D
	xx (kPa)	yy (kPa)
1	39	33
2	52	33
3	71.5	33
4	78	22
5	104	11
6	97.5	16.5
7	104	16.5
8	91	22
9	78	22
10	65	27.5

A .		5 D
	xx (kPa)	yy (kPa)
1	36	33
2	57 33	33
3	85 33	33
4	92	27.5
5	106	22
6	120	11
7	113	22
8	92	27.5
9	78	33
10	50	33

.2.3.

D

A .		0.1 D
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0



A .	0.5 D	
	xx (kPa)	yy (kPa)
1	0	0
2	0	0
3	0	0
4	7	0
5	7	0
6	7	0
7	0	0
8	0	0
9	0	0
10	0	0

A .	D	
	xx (kPa)	yy (kPa)
1	0	5.5
2	0	5.5
3	7	5.5
4	14	0
5	14	0
6	14	0
7	7	5.5
8	7	5.5
9	0	5.5
10	0	5.5

A .	1.5 D	
	xx (kPa)	yy (kPa)
1	1	5.5
2	1	11
3	8.5	11
4	16	11
5	23.5	5.5
6	23.5	5.5
7	23.5	5.5
8	16	5.5
9	8.5	11
10	1	11

A .		2 D
	xx (kPa)	yy (kPa)
1	7	16.5
2	7	16.5
3	14	16.5
4	21	11
5	28	5.5
6	35	5.5
7	28	5.5
8	21	11
9	14	16.5
10	7	16.5

A .		2.5 D
	xx (kPa)	yy (kPa)
1	1	16.5
2	8.5	22
3	16	22
4	31	16.5
5	46	11
6	46	5.5
7	31	16.5
8	23.5	22
9	8.5	22
10	1	16.5

A .		3 D
	xx (kPa)	yy (kPa)
1	0	22
2	7	27.5
3	21	33
4	42	22
5	56	11
6	70	11
7	56	11
8	35	22
9	21	33
10	7	27.5

A .	3.5 D	
	xx (kPa)	yy (kPa)
1	13	36
2	26	36
3	52	24
4	71.5	18
5	78	12
6	65	18
7	52	24
8	26	36
9	13	36
10	6.5	30

A .	4 D	
	xx (kPa)	yy (kPa)
1	0	33
2	14	44
3	35	38.5
4	63	33
5	77	11
6	105	16.5
7	84	21
8	56	33
9	35	38.5
10	14	44

A .	4.5 D	
	xx (kPa)	yy (kPa)
1	14	38.5
2	21	44
3	42	49.5
4	63	38.5
5	91.5	22
6	98	22
7	91.5	27.5
8	56	38.5
9	42	55
10	21	44

A .	5 D	
	xx (kPa)	yy (kPa)
1	14	44
2	35	49.5
3	56	49.5
4	77	38.5
5	105	33
6	112	27.5
7	105	33
8	77	44
9	56	49.5
10	28	49.5

3.

### PHASE 2

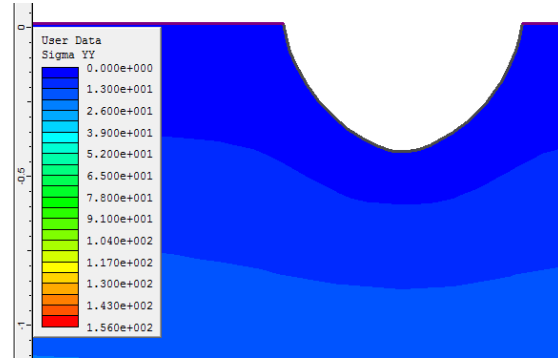
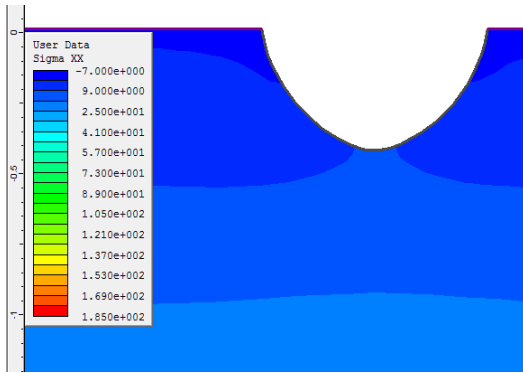
xx yy

D, 2D, 3D, 4D,

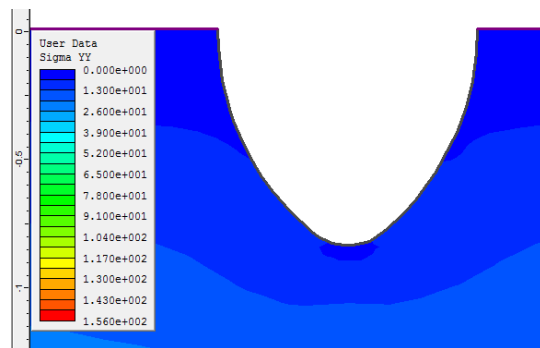
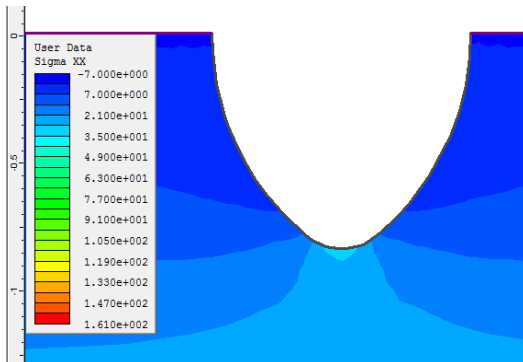
A.3.1.

1/3 D.

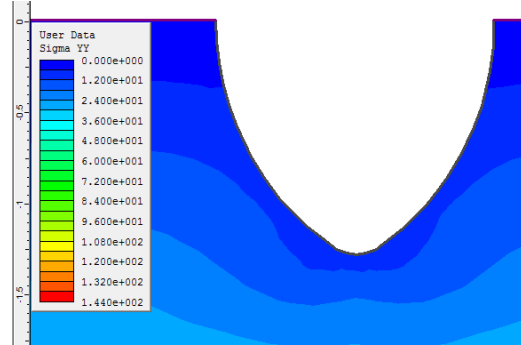
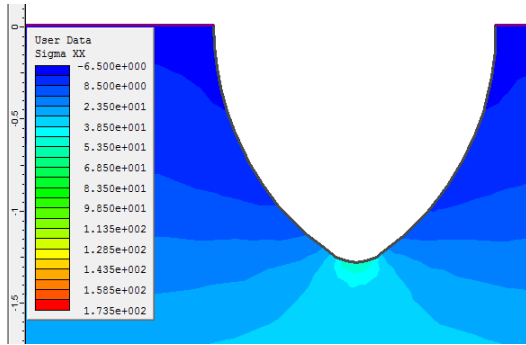
- D



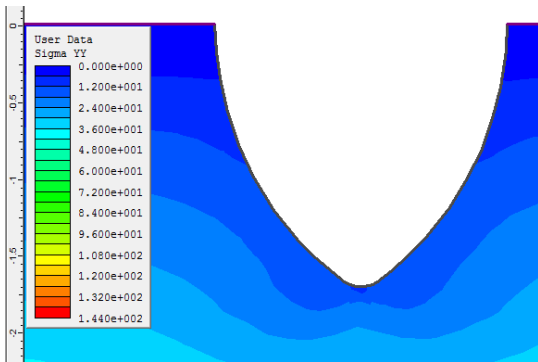
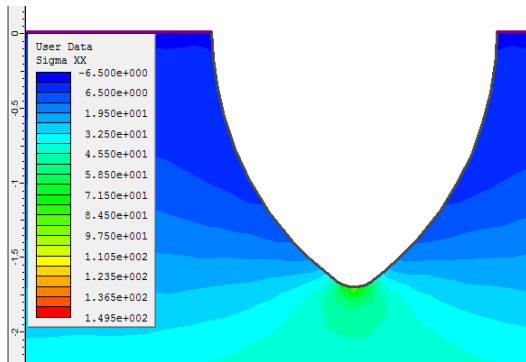
- 2D



- 3D



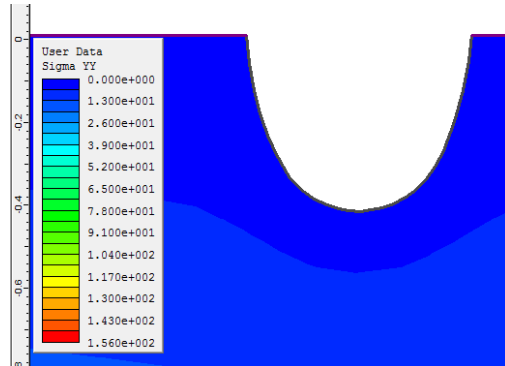
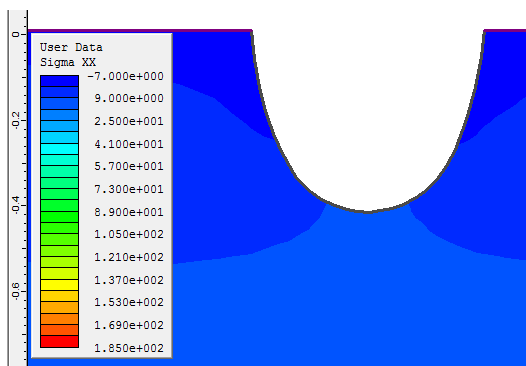
- 4D



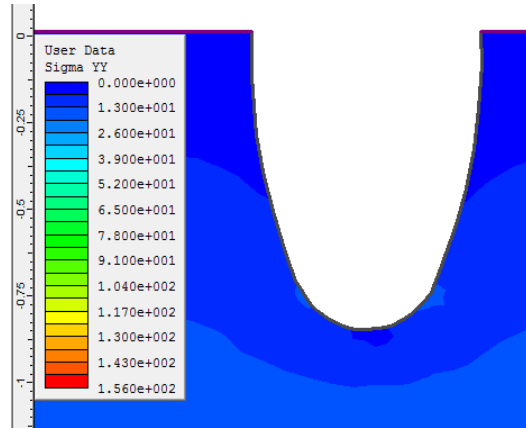
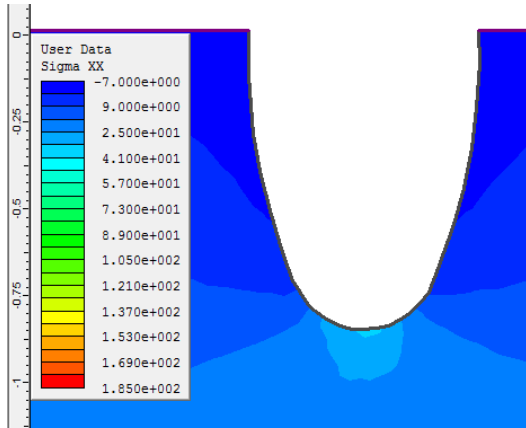
A.3.2.

2/3 D.

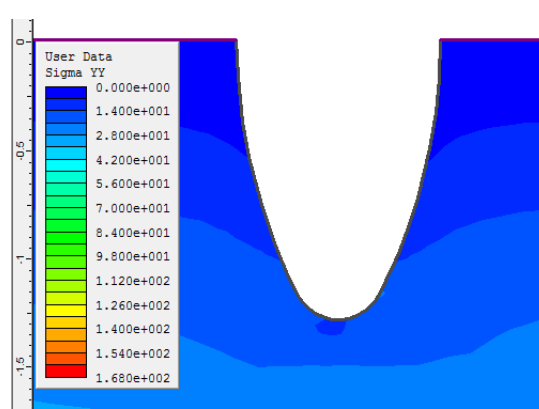
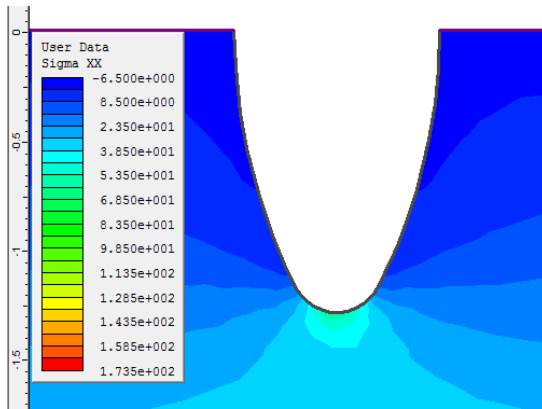
- D



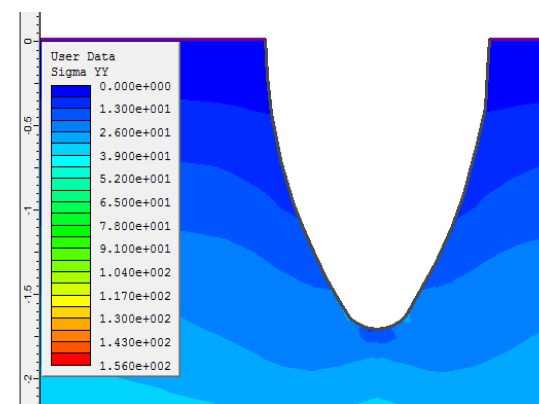
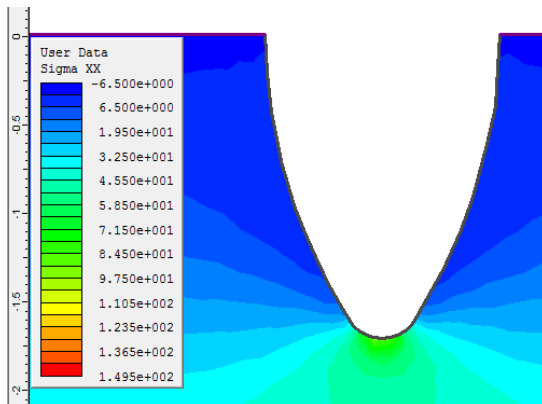
- 2D



- 3D



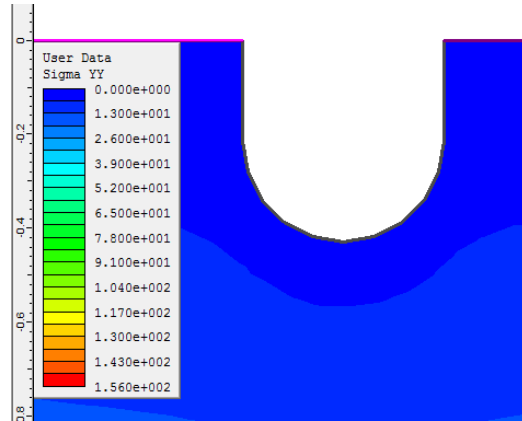
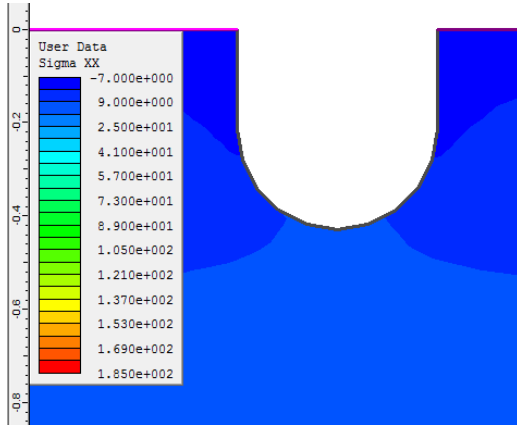
- 4D



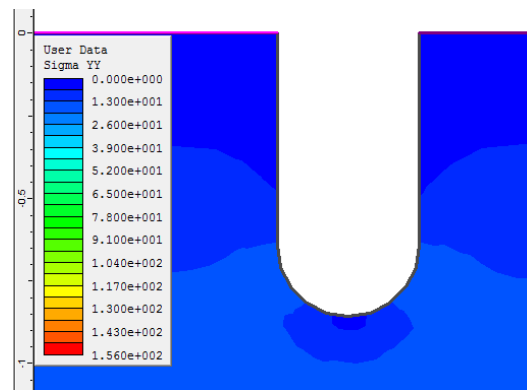
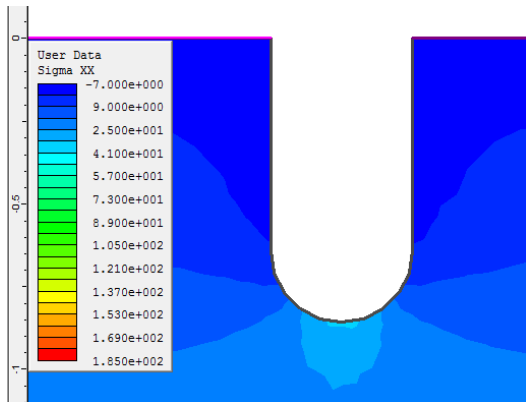
A.3.3.

D.

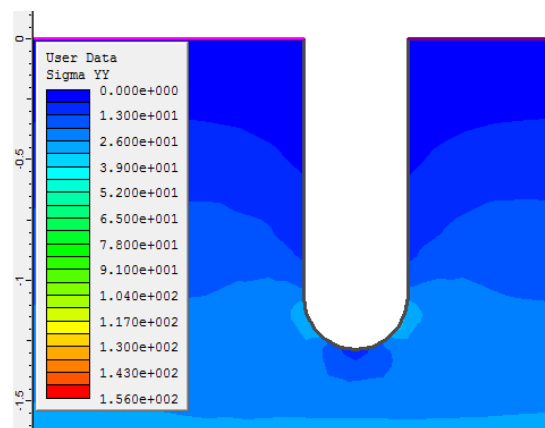
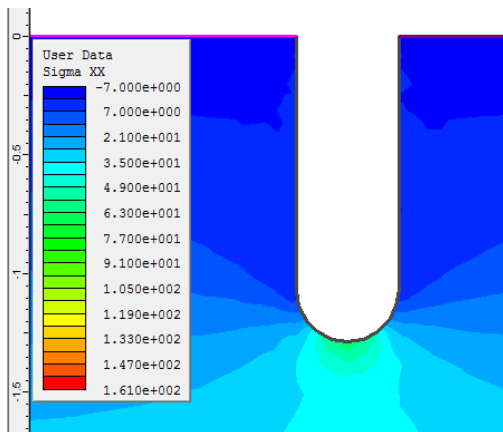
• D



• 2D

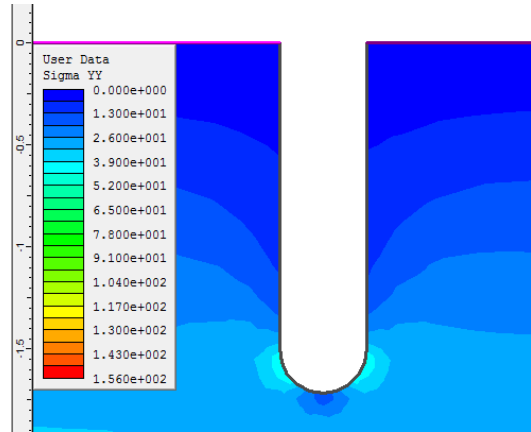
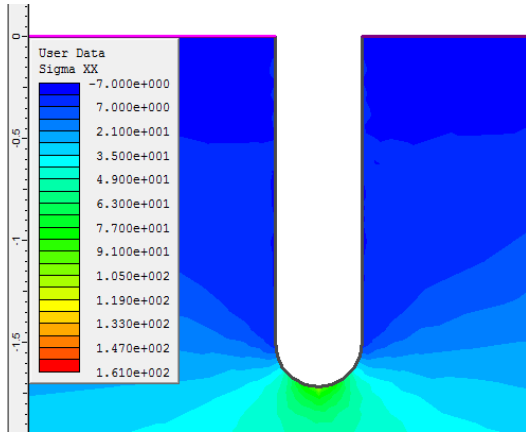


• 3D





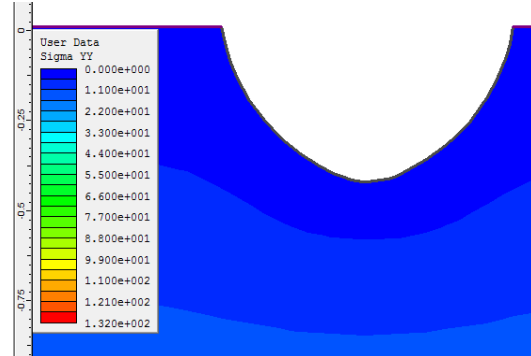
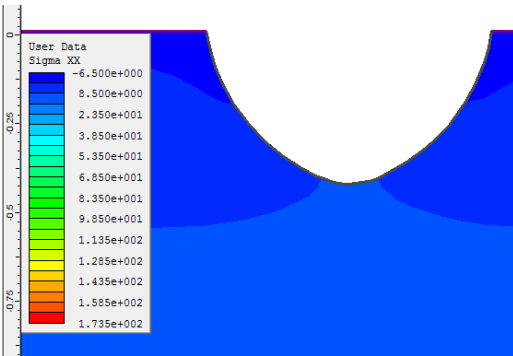
- 4D



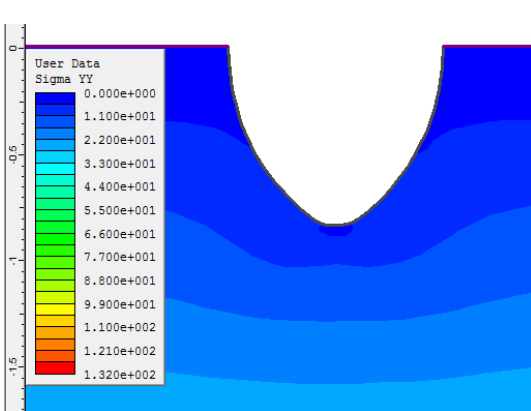
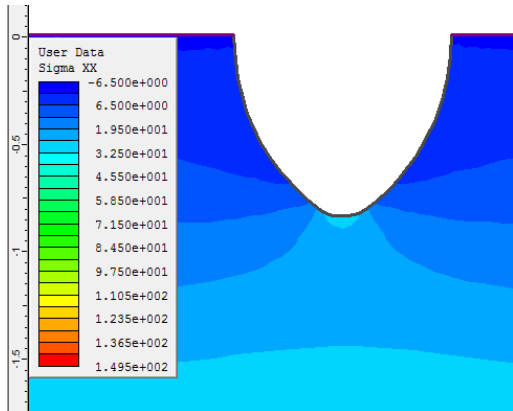
A.3.4.

1/3 D.

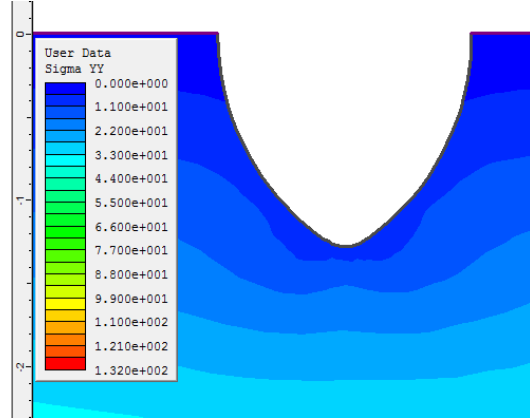
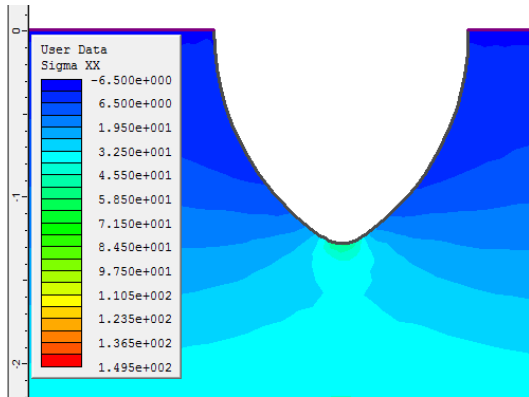
- D



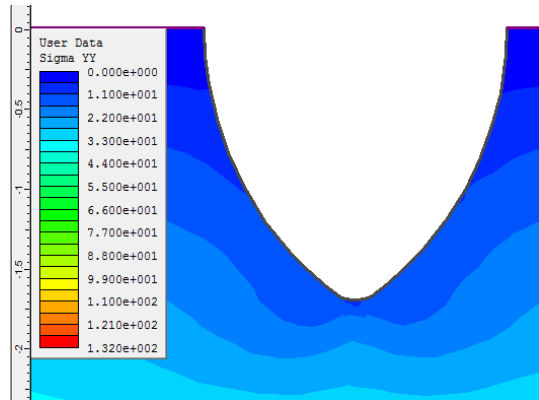
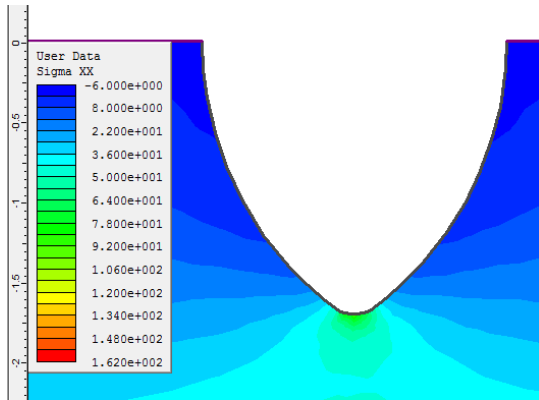
- 2D



- 3D



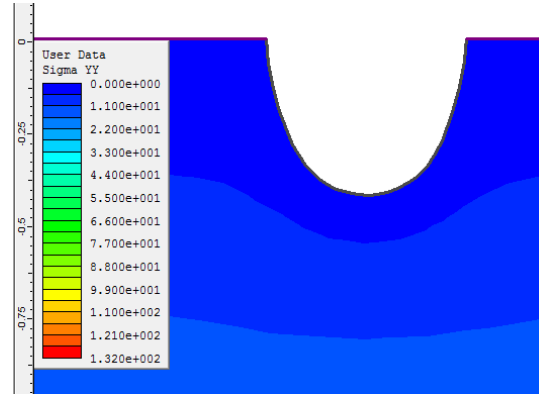
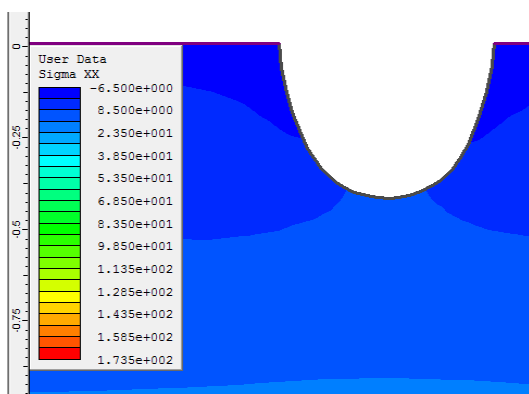
- 4D



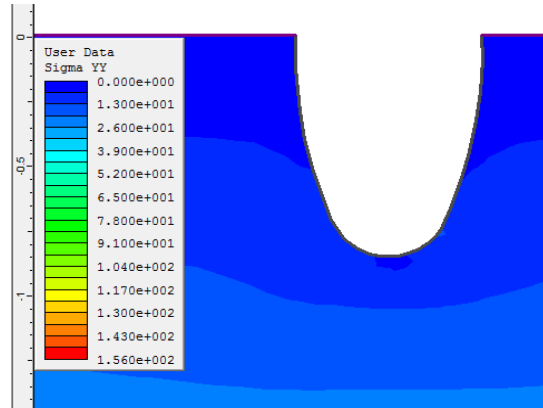
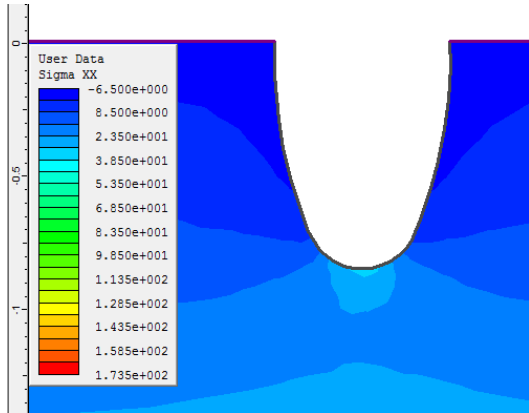
A.3.5.

2/3 D.

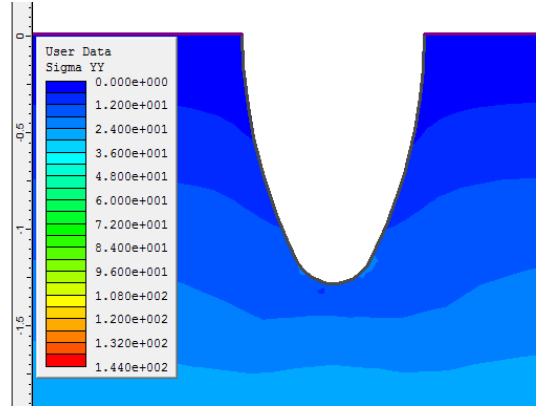
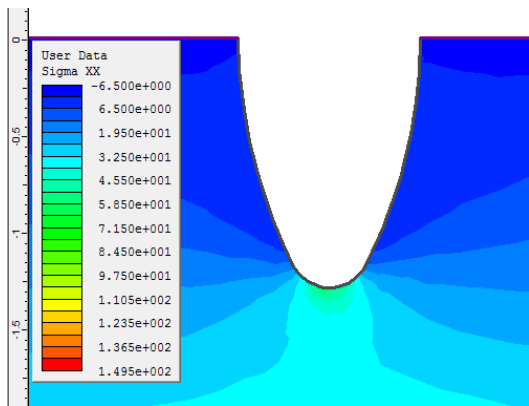
- D



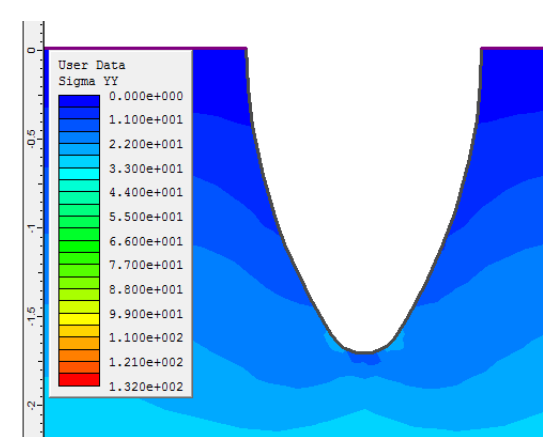
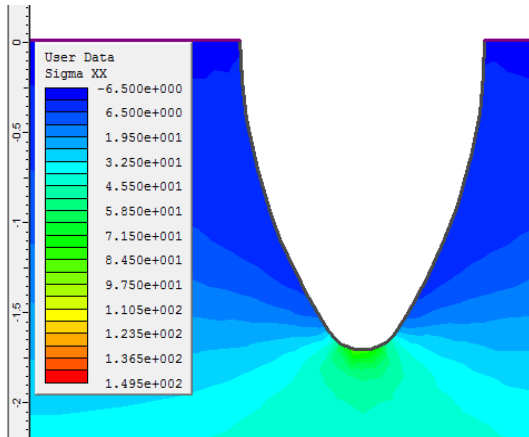
- 2D



- 3D



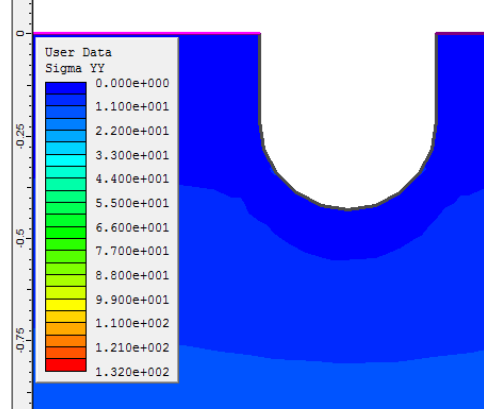
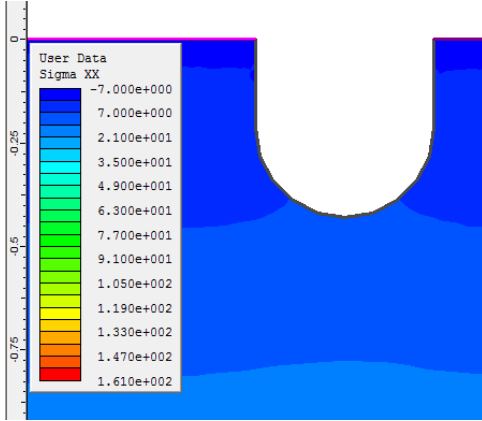
- 4D



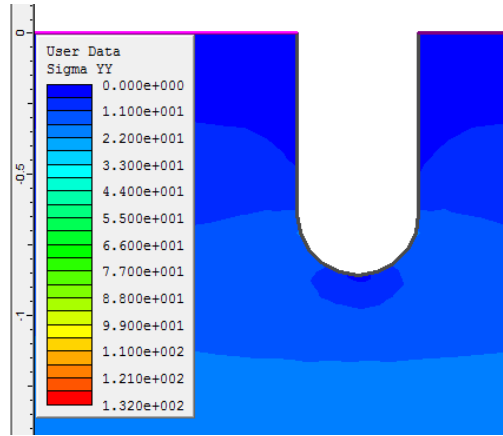
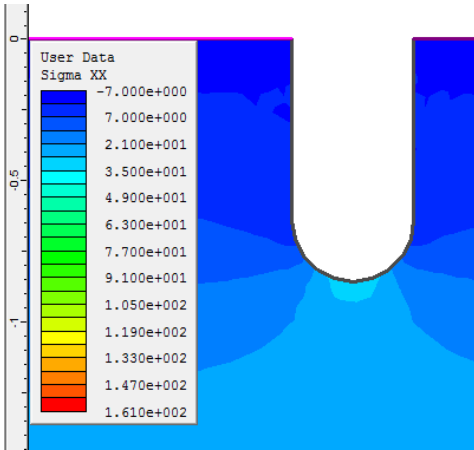
A.3.6.

D.

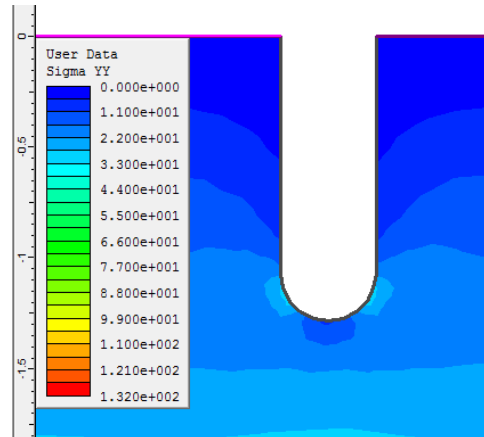
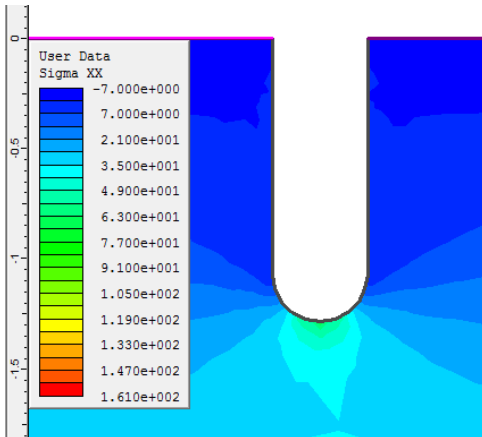
- D



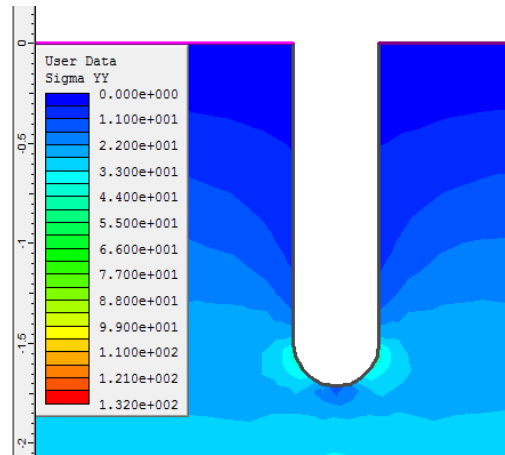
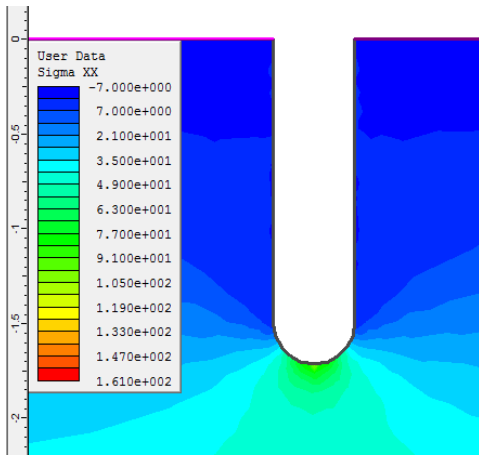
- 2D



- 3D



- 4D



.4.

I

		P (kN/m)		
y/D	y (m)	- , 1/3 D	- , 2/3 D	- , D
0,1	0,0429	0,000	0,000	0,000
0,5	0,2145	0,000	0,001	0,000
1	0,429	0,000	0,463	0,588
1,5	0,6435	0,641	1,145	2,423
2	0,858	1,095	2,515	2,992
2,5	1,0725	1,288	3,575	3,899
3	1,287	1,797	4,340	6,138
3,5	1,5015	2,437	3,930	7,388
4	1,716	2,592	5,268	9,150
4,5	1,9305	2,830	7,359	11,130
5	2,145	3,252	8,396	12,590

		P (kN/m)		
y/D	y (m)	- , 1/3 D	- , 2/3 D	- , D
0,1	0,0429	0,000	0,000	0,000
0,5	0,2145	0,000	0,000	0,000
1	0,429	0,000	0,994	0,960
1,5	0,6435	0,733	1,544	2,576
2	0,858	1,332	2,697	3,882
2,5	1,0725	1,500	4,226	4,134
3	1,287	1,800	5,312	6,304
3,5	1,5015	2,200	5,879	7,294
4	1,716	2,503	6,300	9,466
4,5	1,9305	3,445	7,170	11,517
5	2,145	3,821	9,041	13,649



CON3DF

10

4

- $x = 1 \text{ m}, z = 0 \text{ m}, \omega = 0.2 \text{ rad/sec}$
- $x = 0 \text{ m}, z = 1 \text{ m}, \omega = 0.2 \text{ rad/sec}$
- $x = 1 \text{ m}, z = 0 \text{ m}, \omega = 0.6 \text{ rad/sec}$
- $x = 0 \text{ m}, z = 1 \text{ m}, \omega = 0.6 \text{ rad/sec}$

2

rad/sec)

(2/3)D,

5.

5, 2D, 2.5D, 4D.

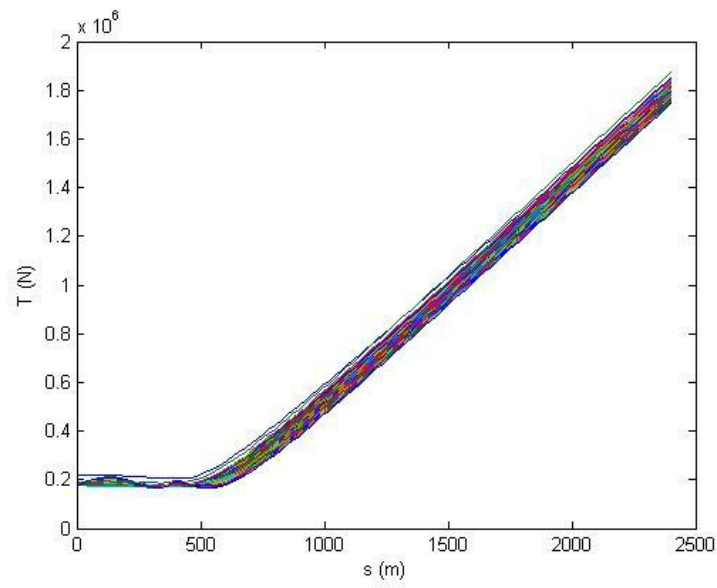
(x = 1,  $\omega = 1 \text{ rad/sec}$  z = 1,  $\omega = 1$

5



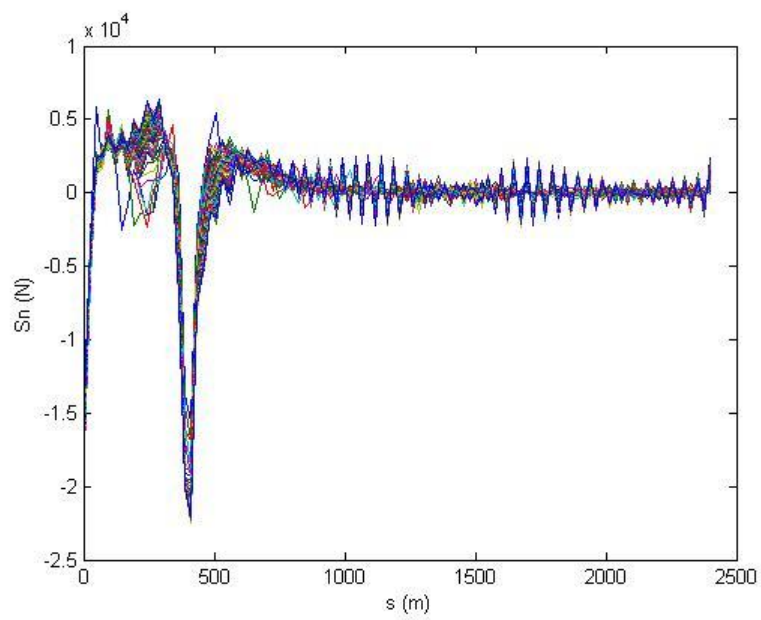
.1

:  $x = 1 \text{ m}$ ,  $z = 0 \text{ m}$ ,  $\omega = 0.2 \text{ rad/sec}$



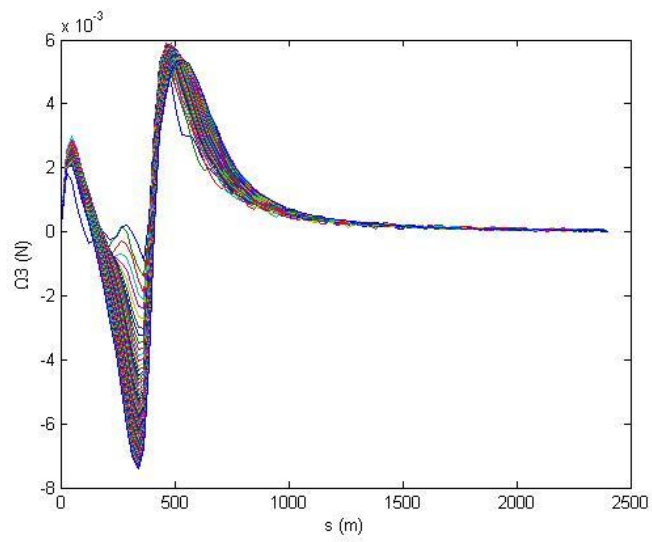
.1.1

T  
2D



.1.2

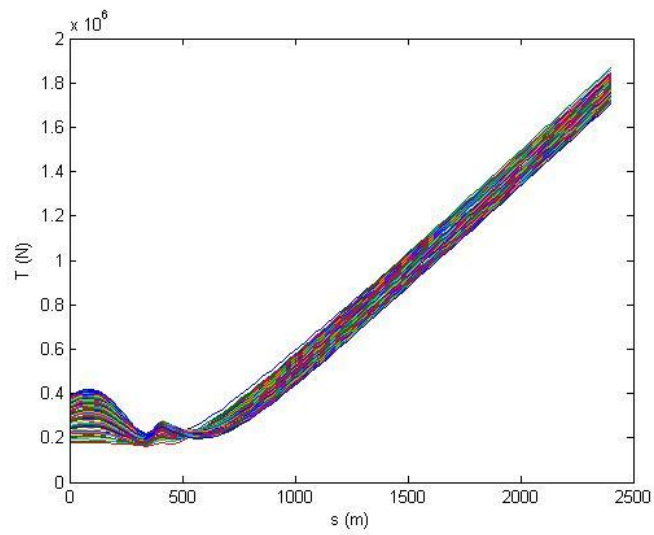
$S_n$   
2D



.1.3

3

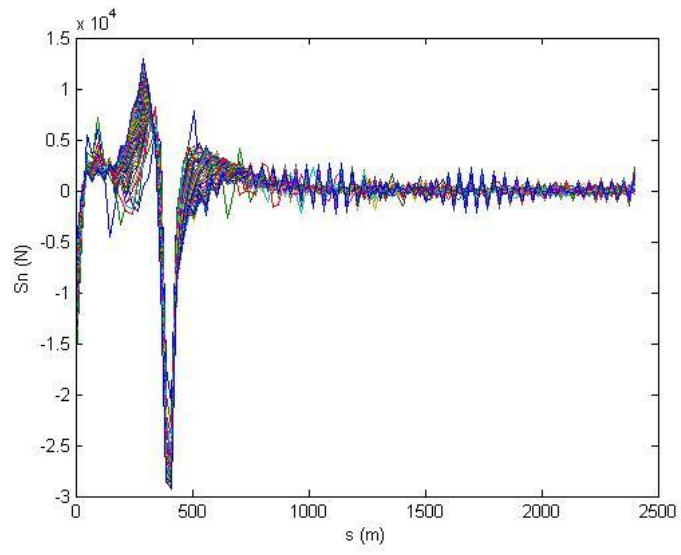
2D



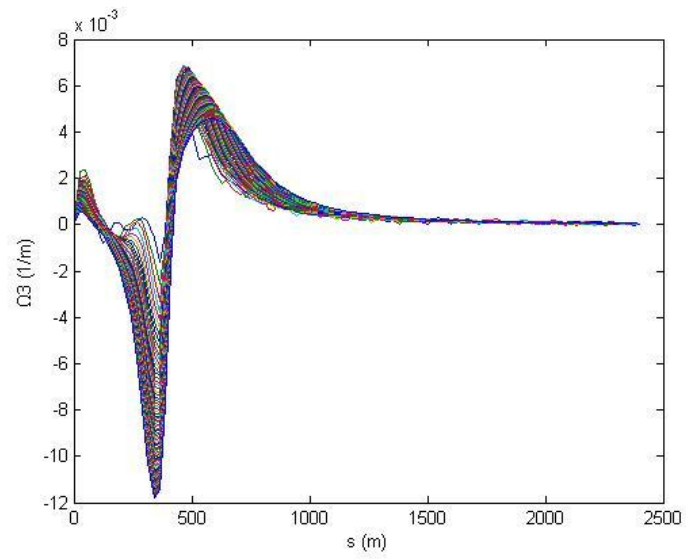
.1.4

$T$

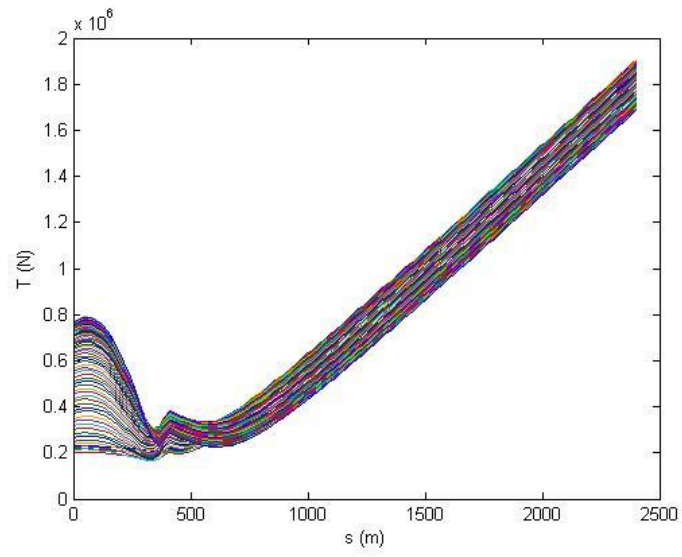
2.5D



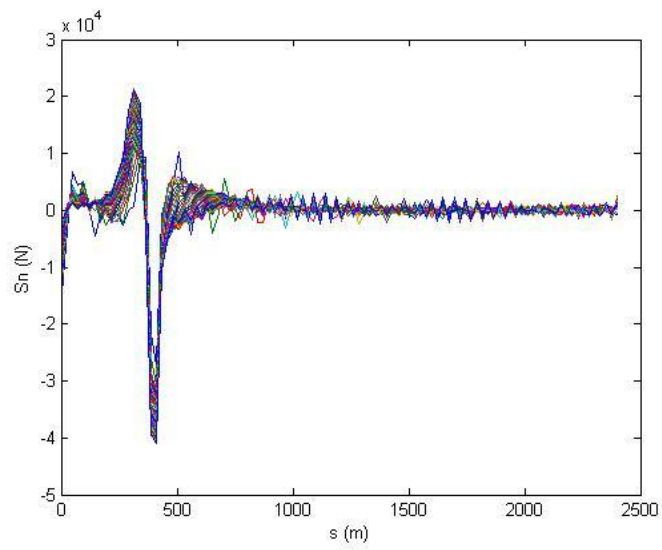
.15                      Sn  
2.5D



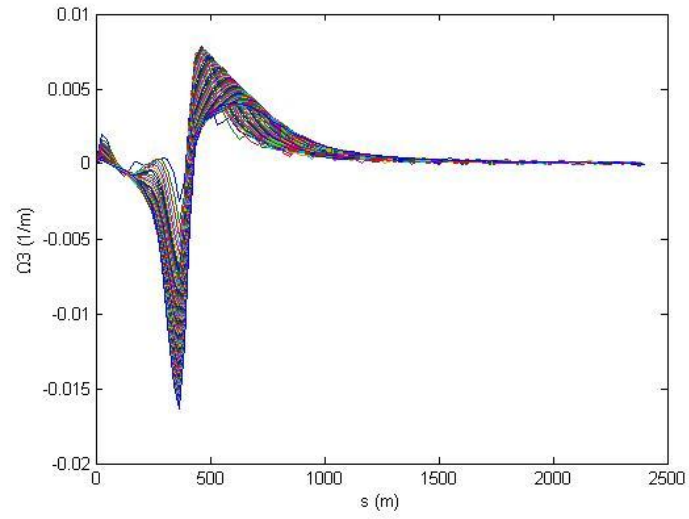
.16                      3  
2.5D



.1.7  $T$   
4D

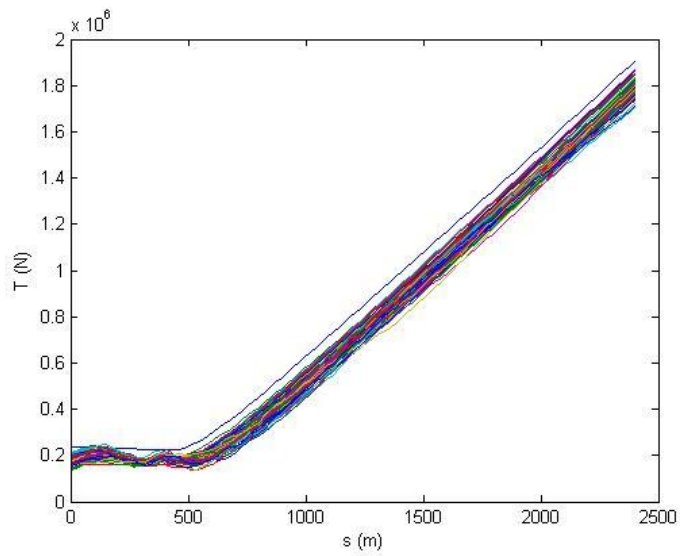


.1.8  $S_n$   
4D

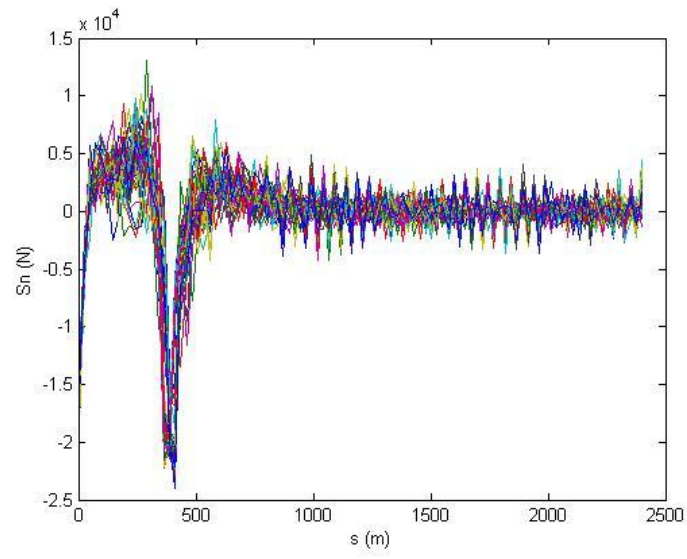


.1.9                      3  
4D

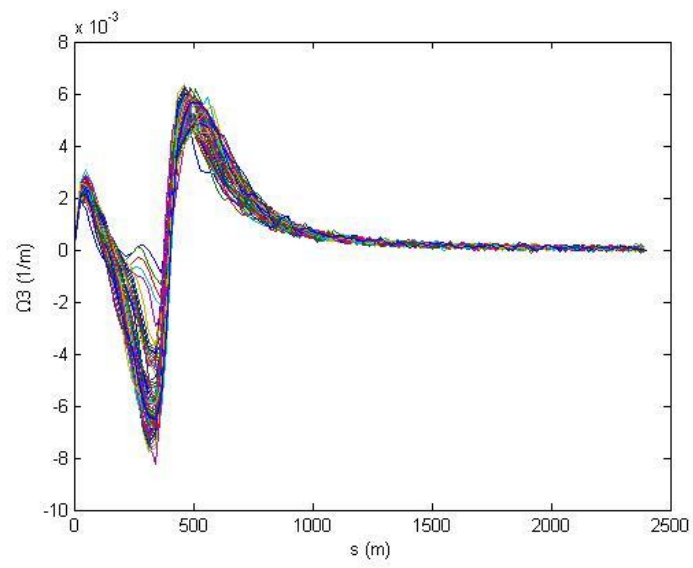
- :  $x = 0$  m,  $z = 1$  m,  $\omega = 0.2$  rad/sec



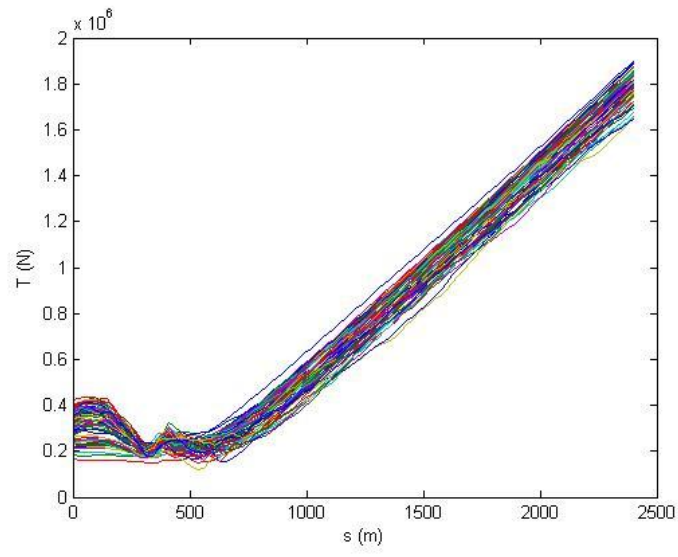
.1.10                      T  
2D



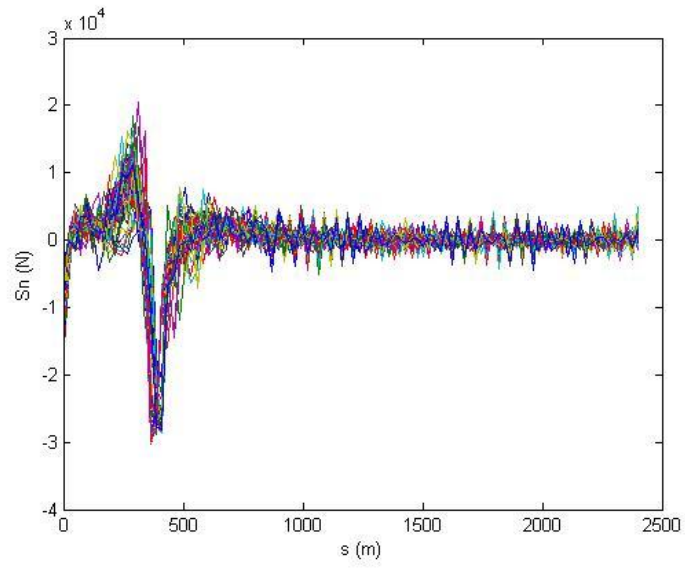
.1.11                       $S_n$   
2D



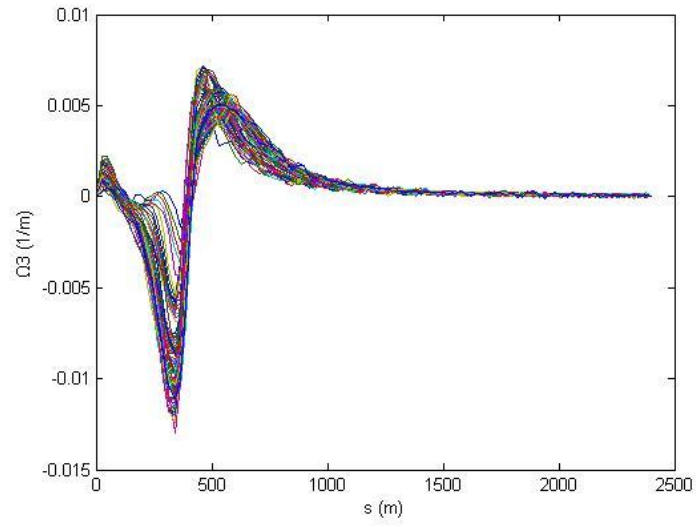
.1.12                      3  
2D



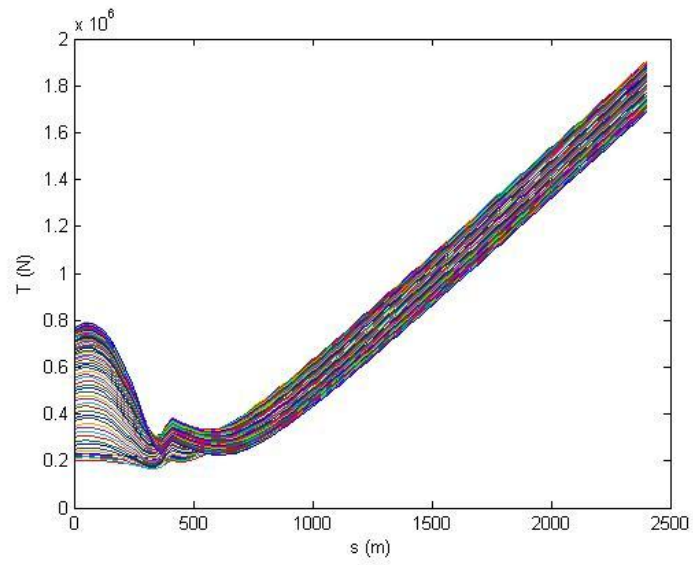
.1.13  $T$   
2.5D



.1.14  $S_n$   
2.5D

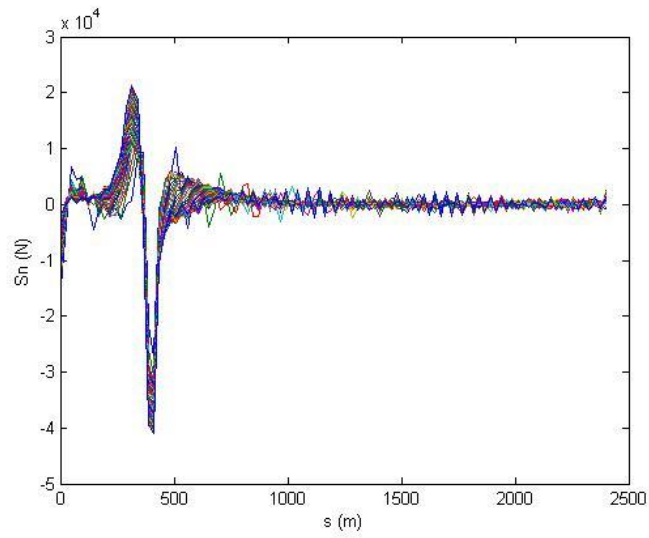


.1.15                      3  
2.5D

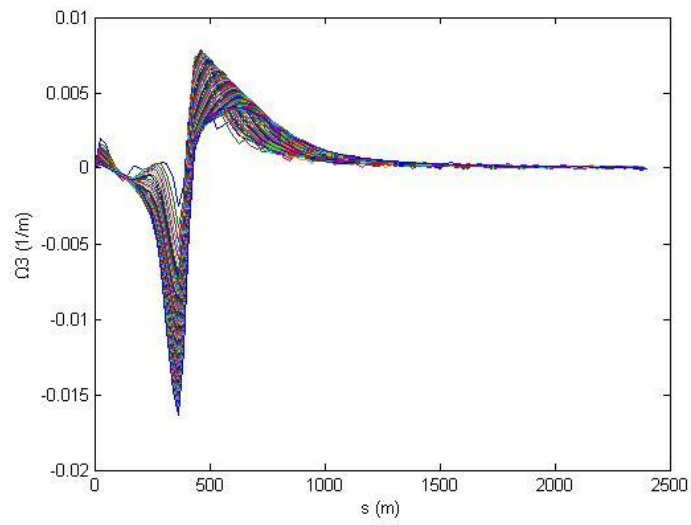


.1.16                      *T*  
4D



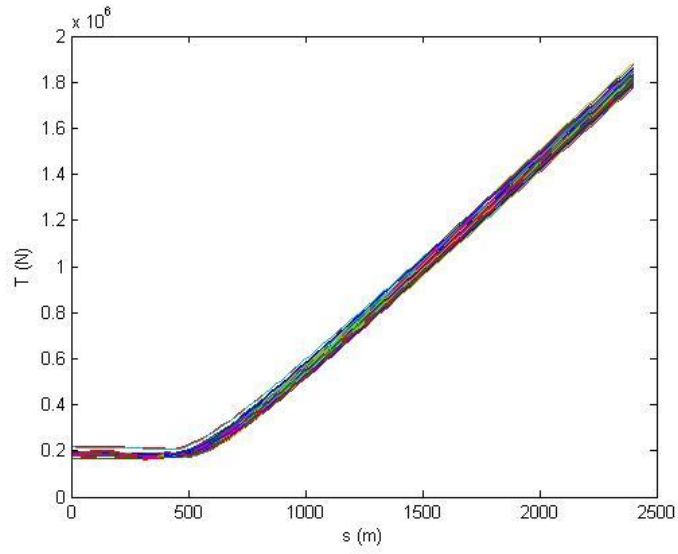


.1.17                      Sn  
4D

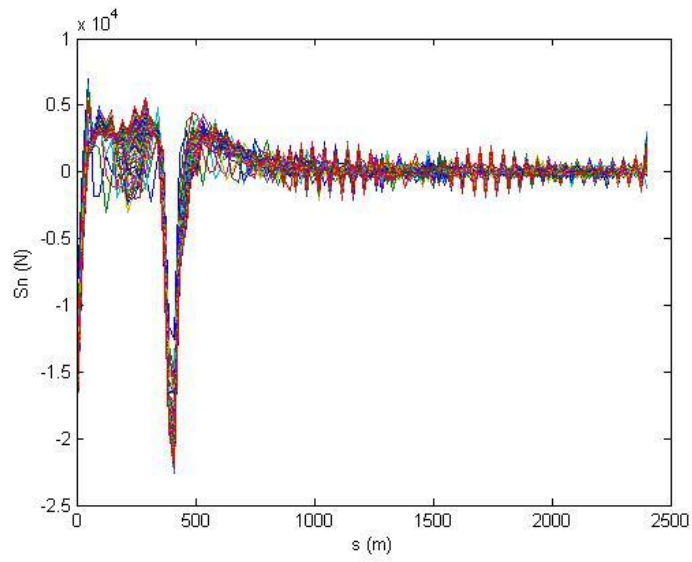


.1.18                      3  
4D

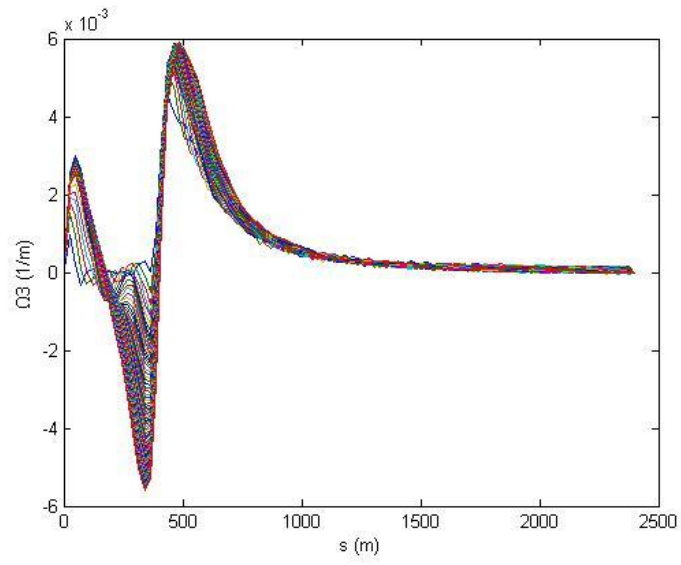
- :  $x = 1 \text{ m}$ ,  $z = 0 \text{ m}$ ,  $\omega = 0.6 \text{ rad/sec}$



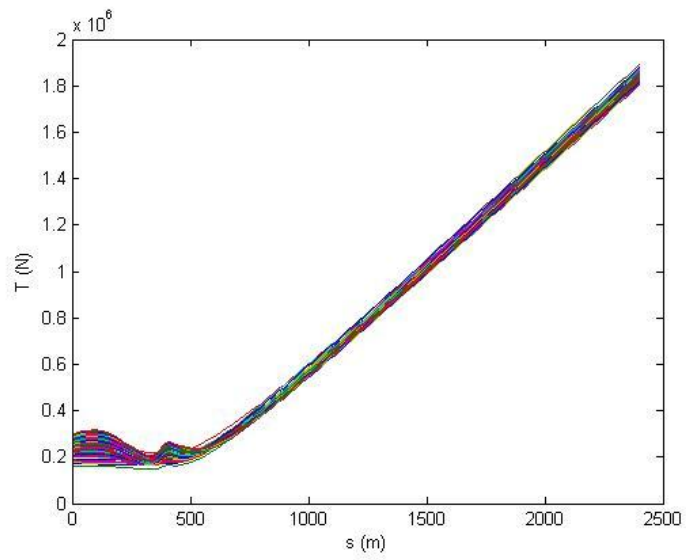
.1.19 T  
2D



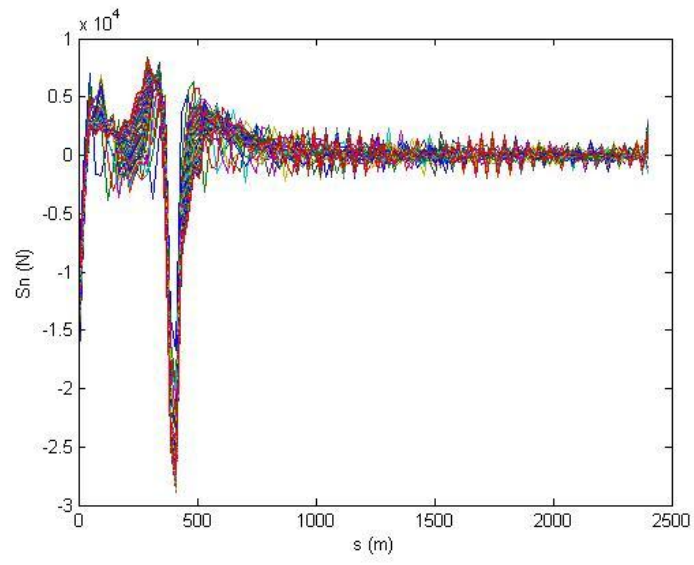
.1.20 Sn  
2D



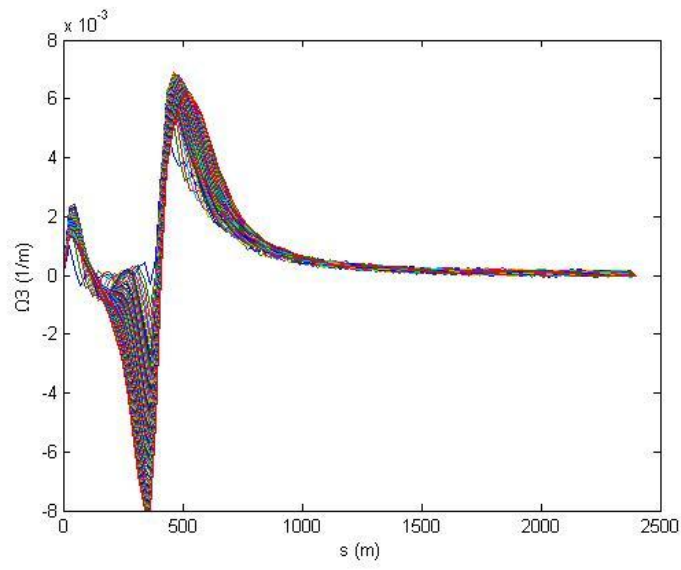
.1.21                      3  
2D



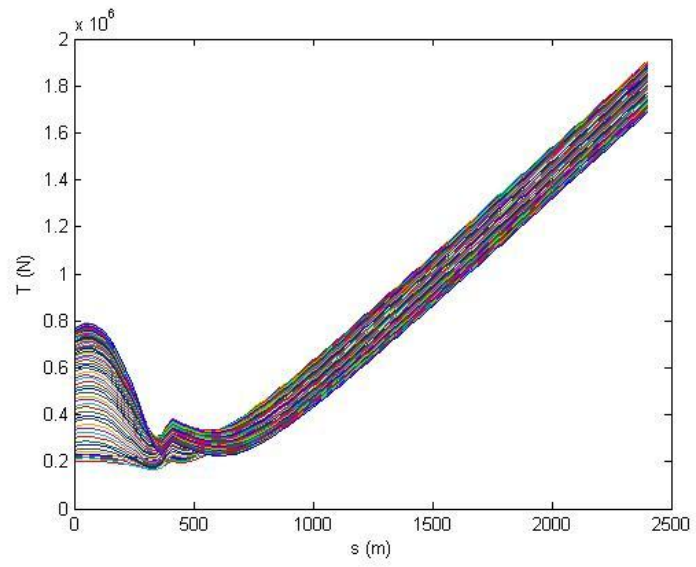
.1.22                       $T$   
2.5D



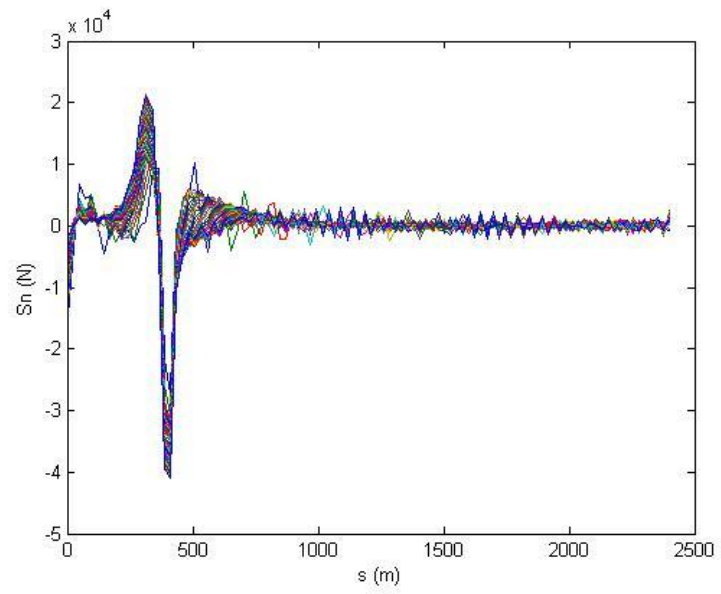
.1.23                      Sn  
2.5D



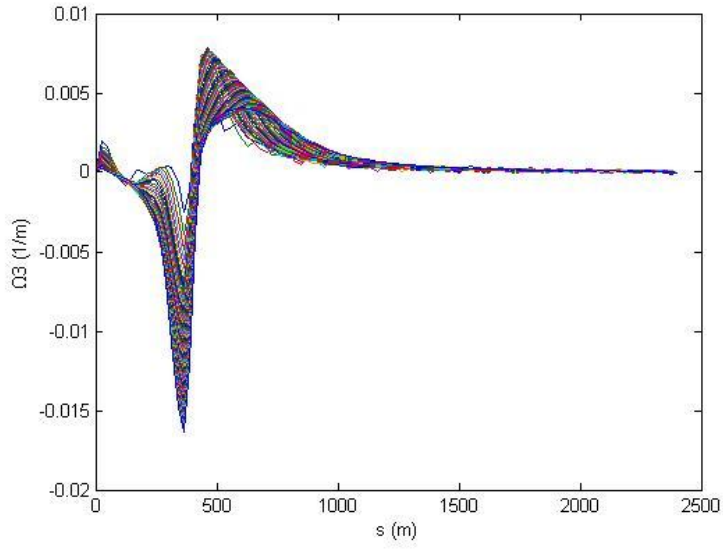
.1.24                      3  
2.5D



.1.25  $T$   
4D

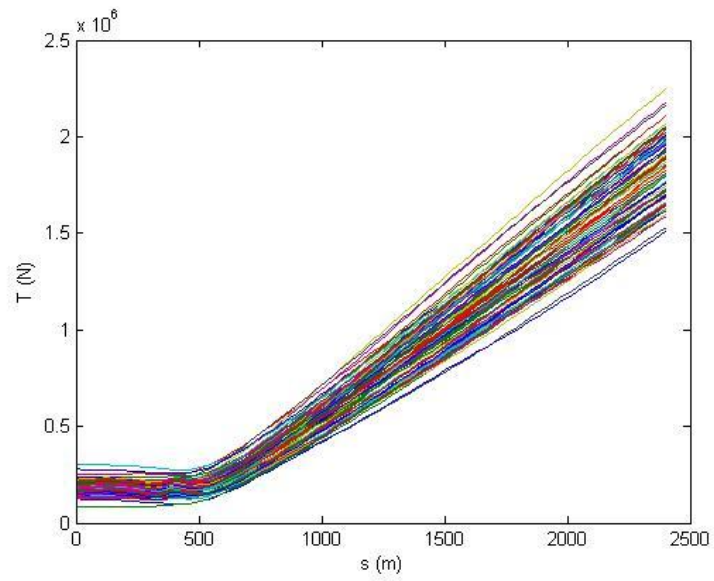


.1.26  $S_n$   
4D

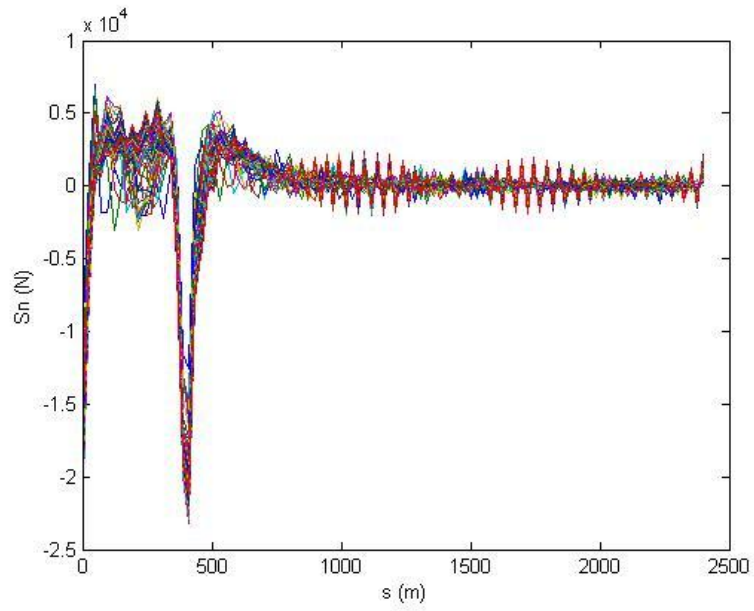


.1.27                      3  
4D

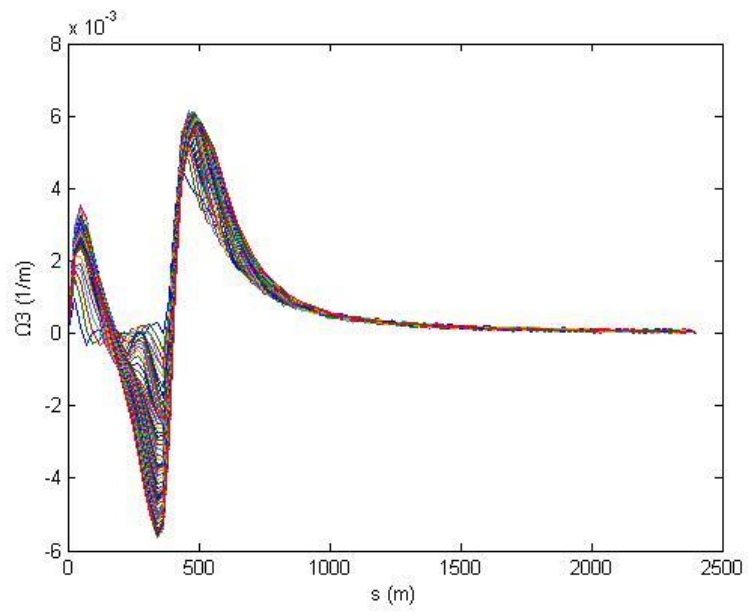
- :  $x = 0 \text{ m}$ ,  $z = 1 \text{ m}$ ,  $\omega = 0.6 \text{ rad/sec}$



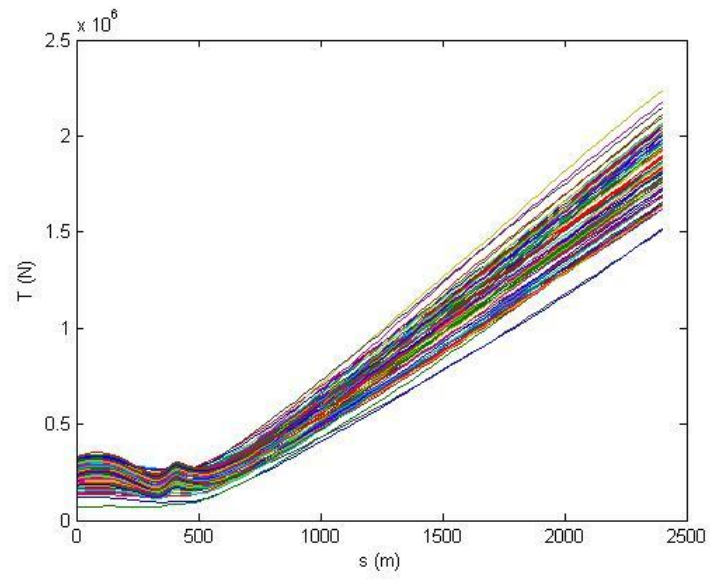
.1.28                      T  
2D



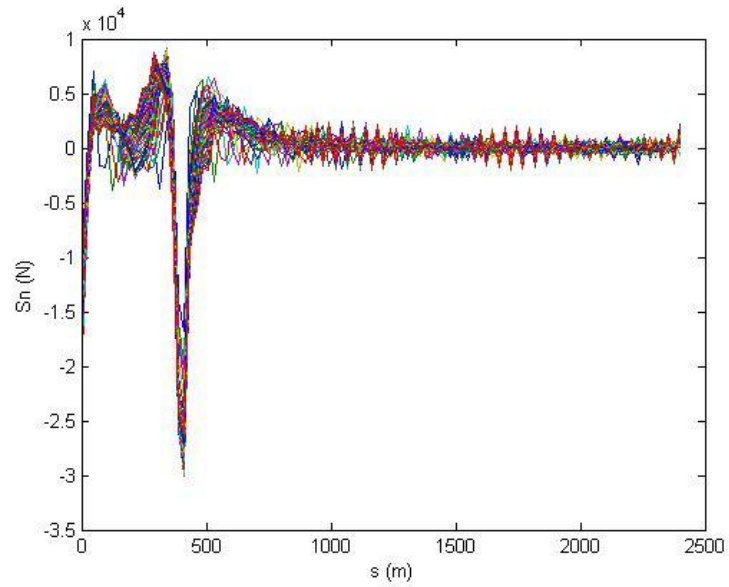
.1.29 Sn  
2D



.1.30 3  
2D

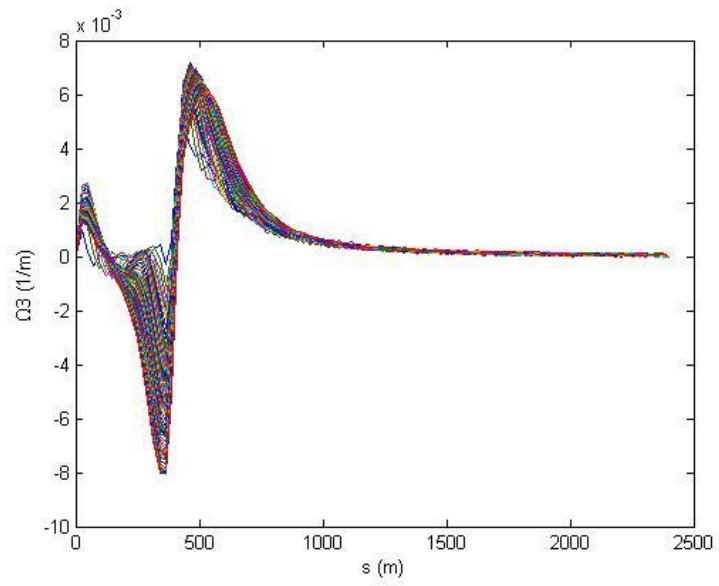


.1.31  $T$   
2.5D



.1.32  $S_n$   
2.5D

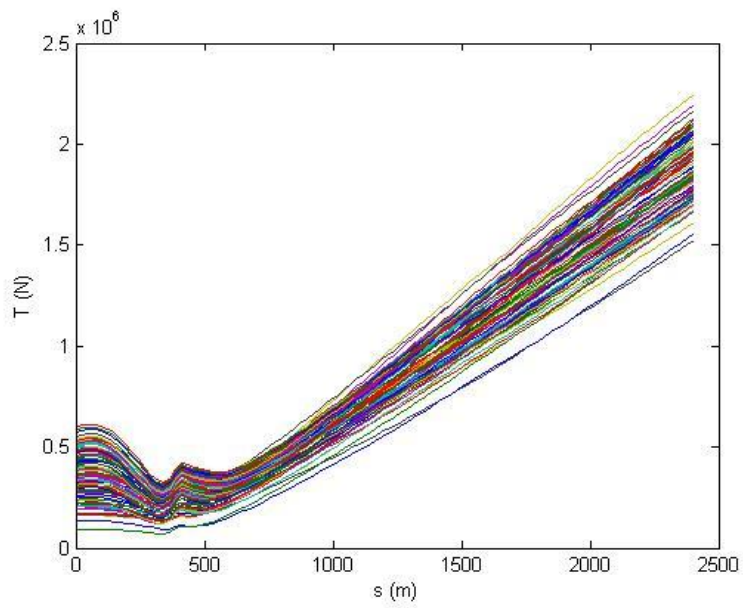




.1.33

3

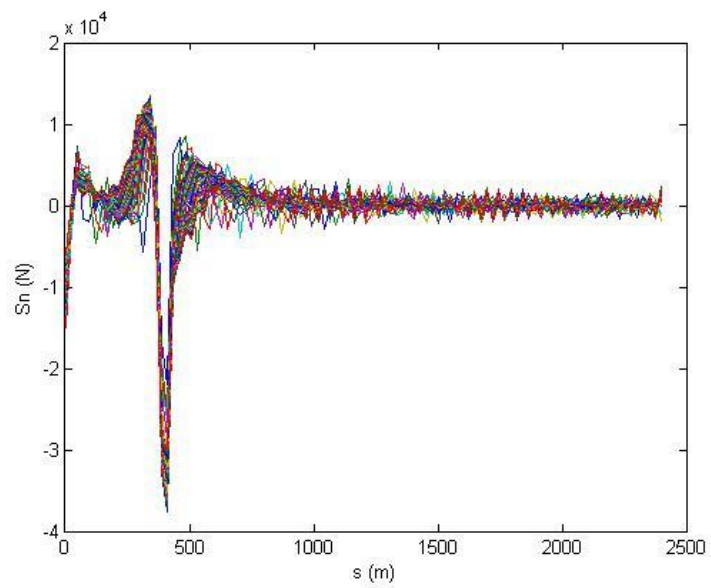
2.5D



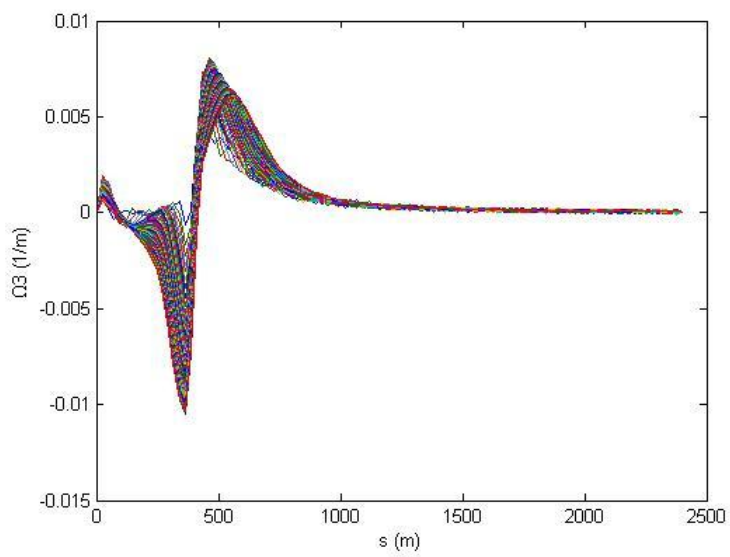
.1.34

$T$

4D



.1.35                      Sn  
4D



.1.36                      3  
4D



SCR - Steel Catenary Riser,

"sagbend"

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TDP)

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(in-plane)

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4.1.8.

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TDP

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TDZ.

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"function file"

2 "function file"

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function files,  
(BVPINIT)

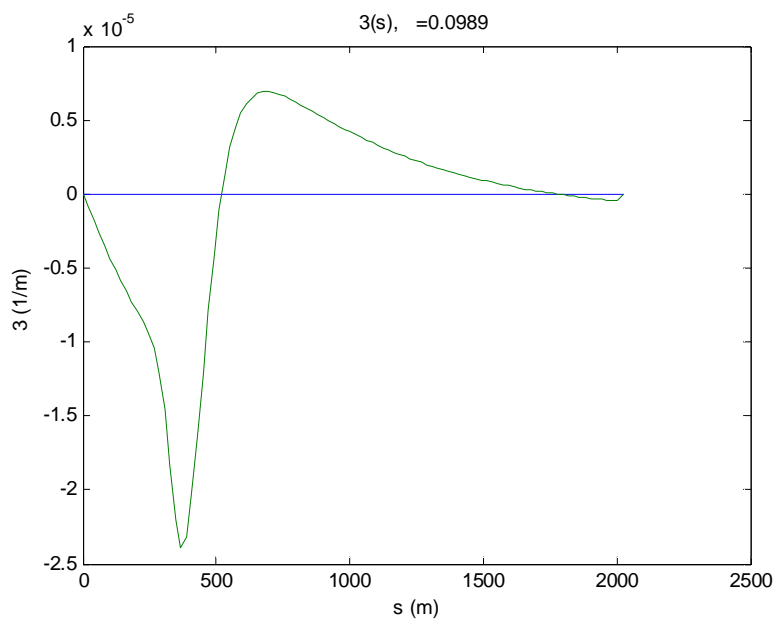
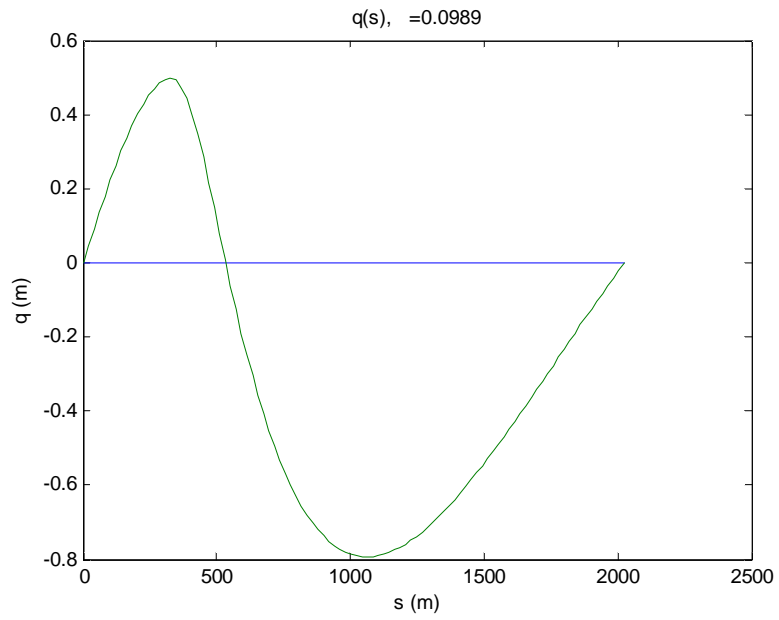
(BVP4C)

( . . . ) .

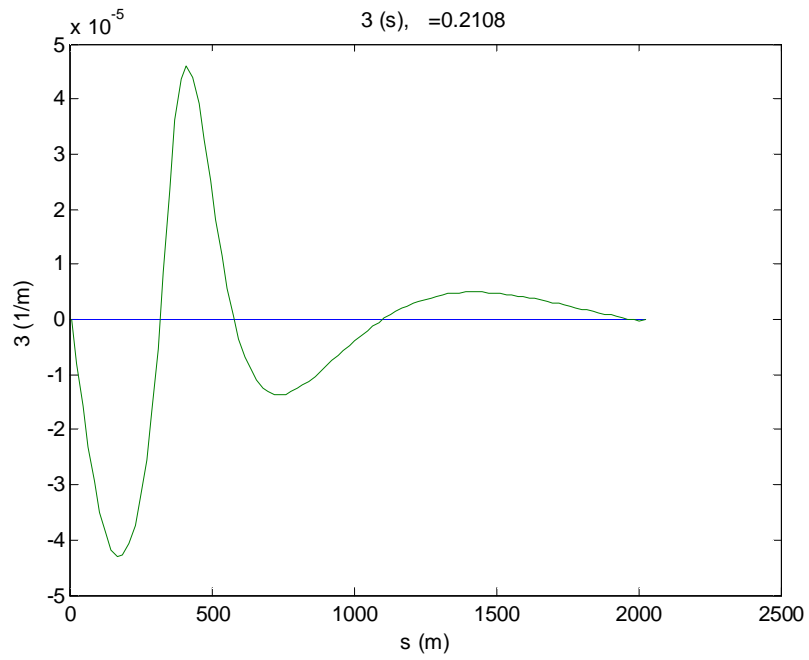
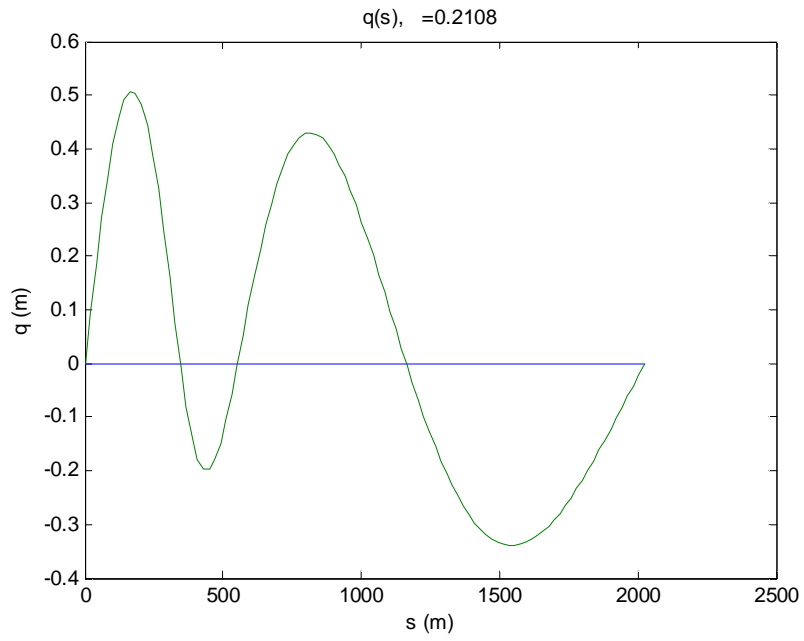
3, , q, (out-of-plane),

5, TDP TDZ,

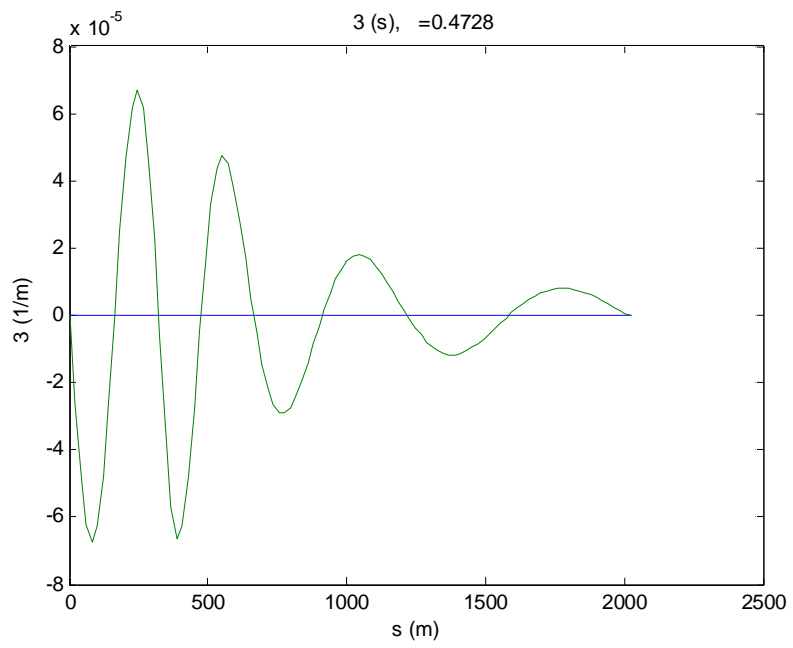
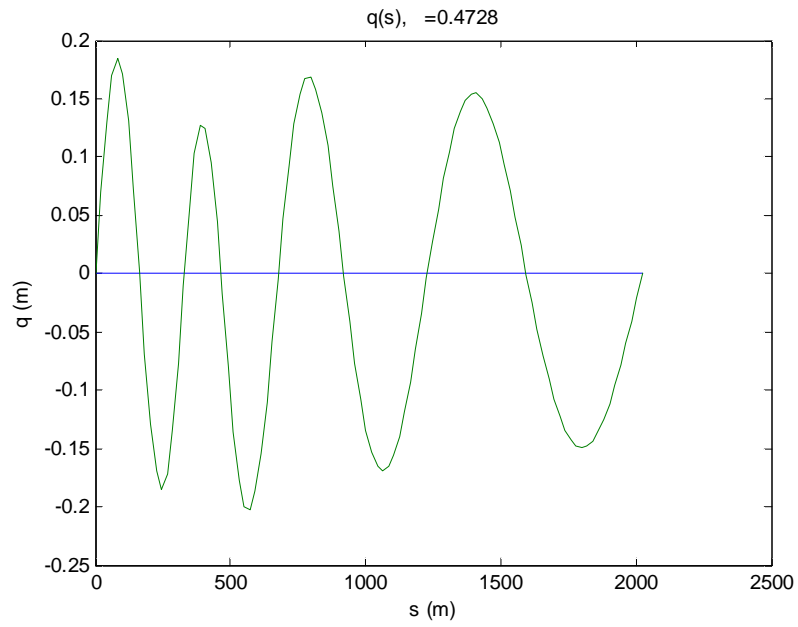
- 1 , =0.0989



- 2 ,  $\nu = 0.2108$

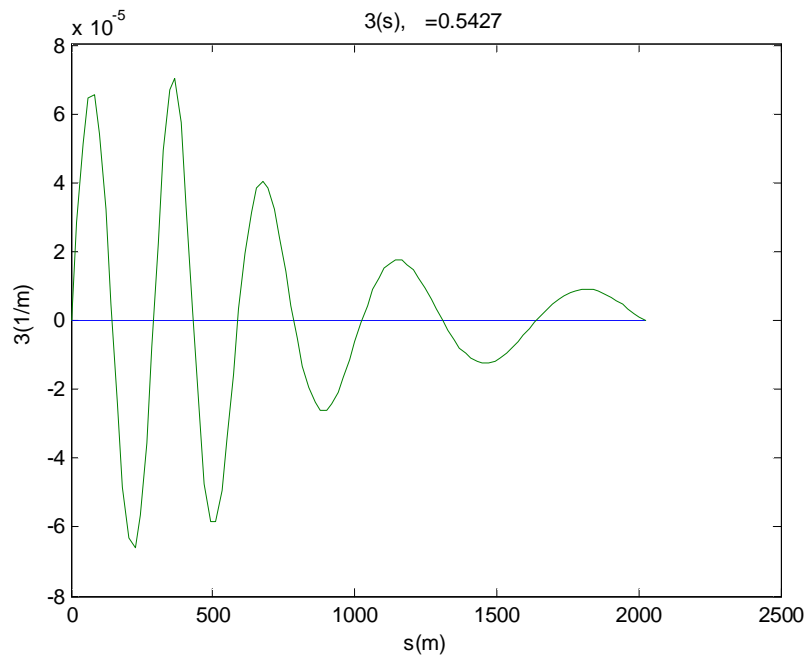
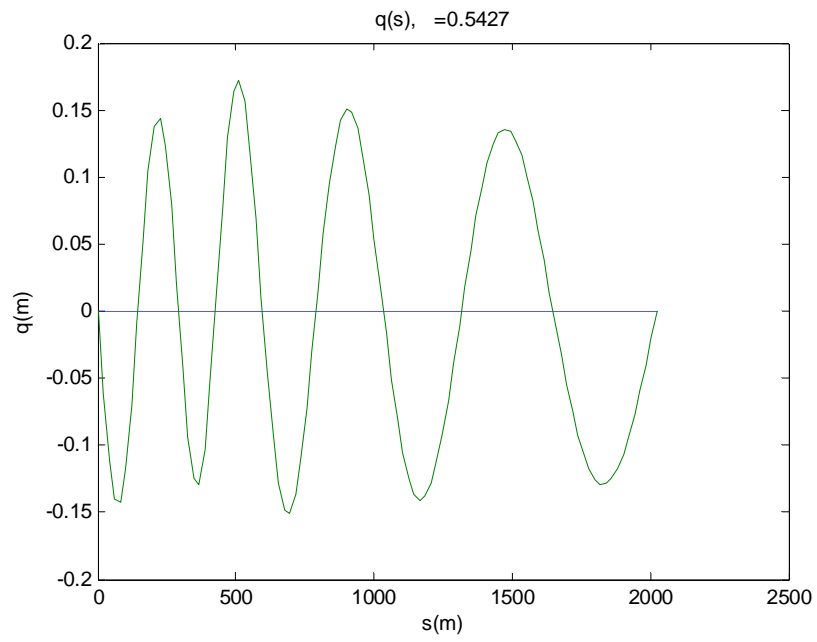


- 3 ,  $\lambda = 0.4728$

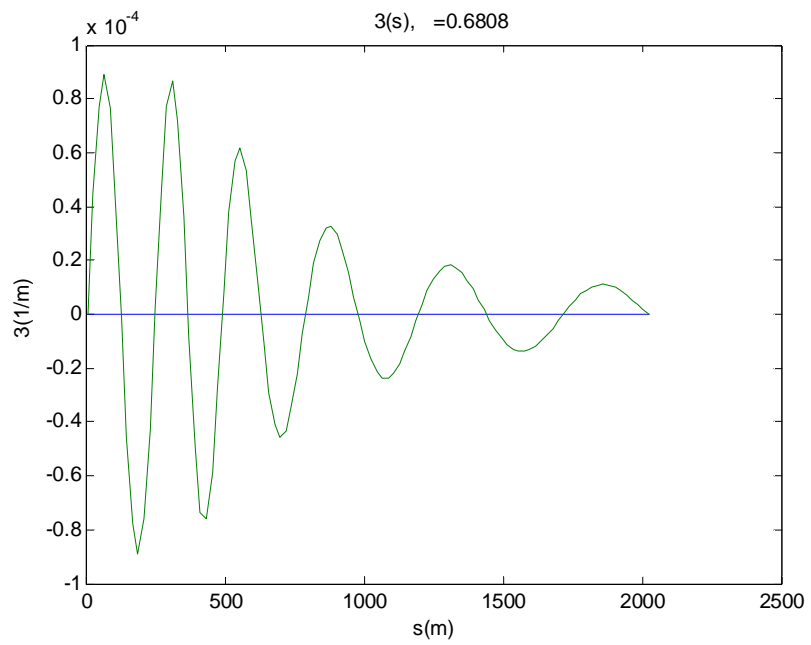
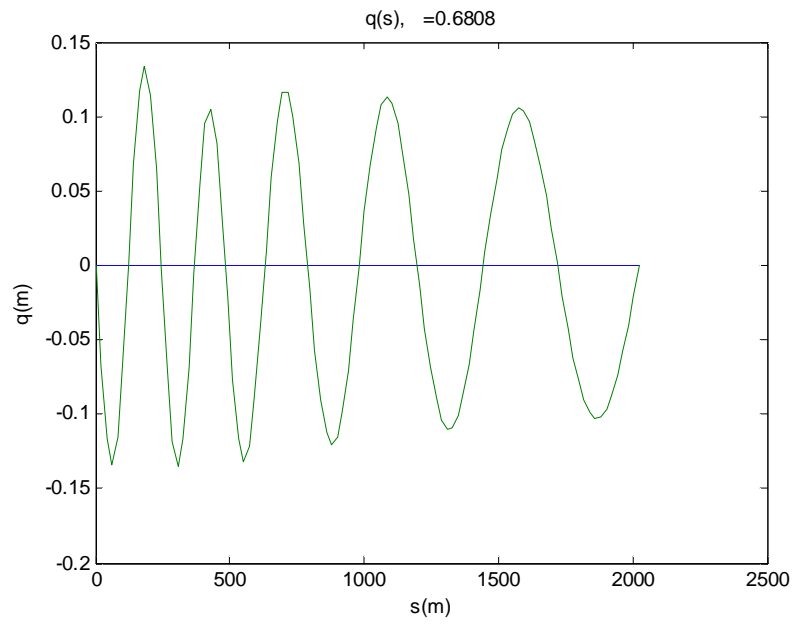




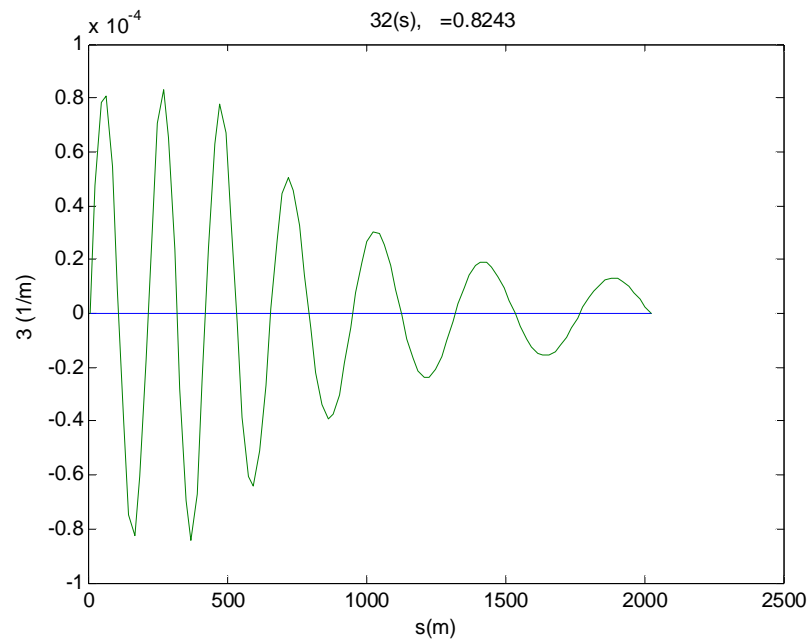
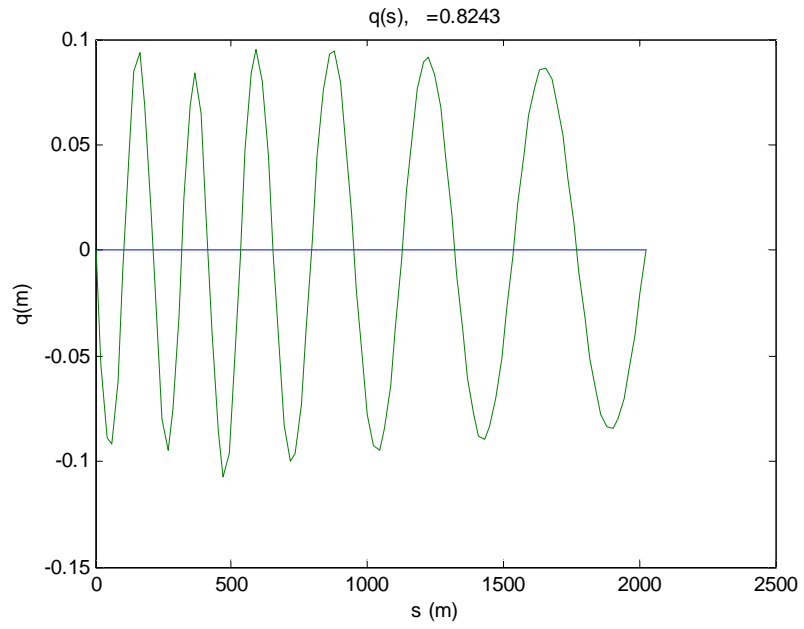
- 4 ,  $\omega = 0.5427$



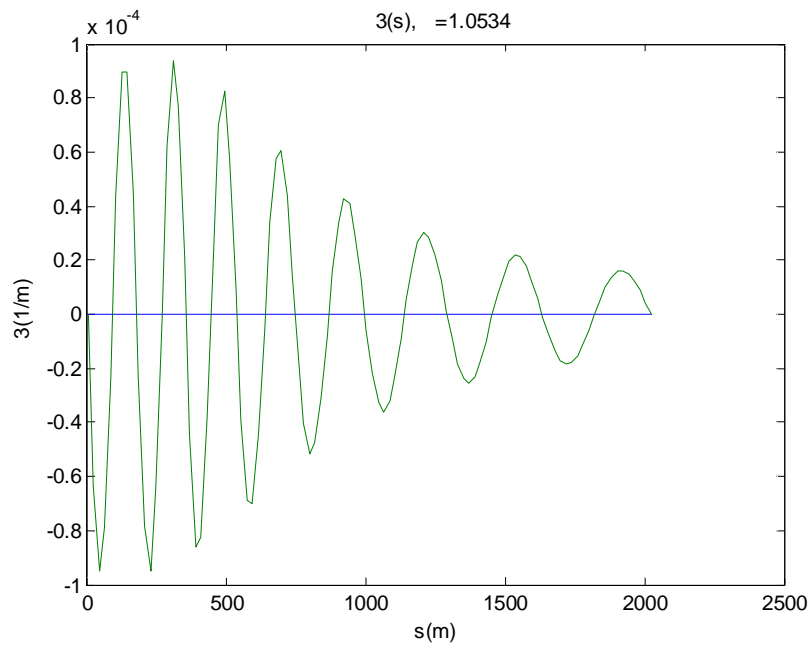
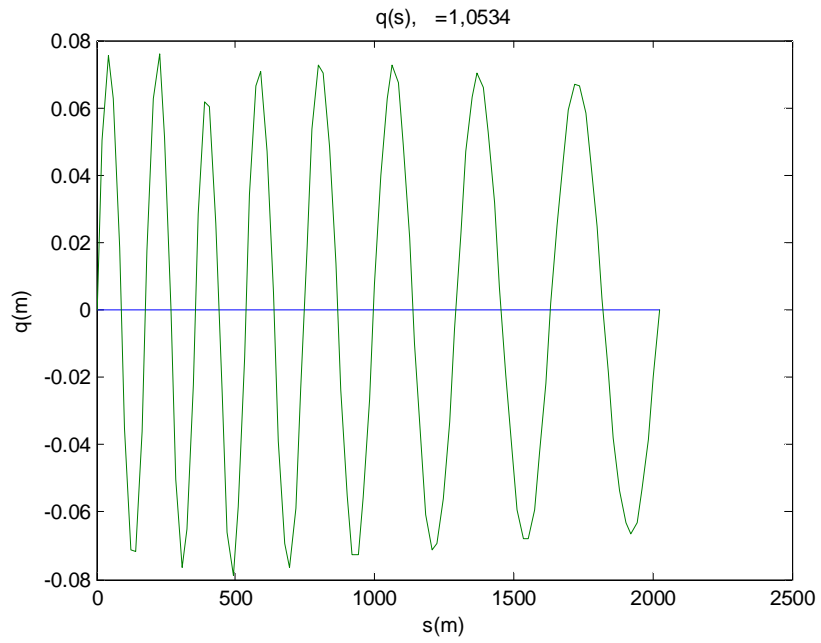
- 5 ,  $\omega = 0.6808$



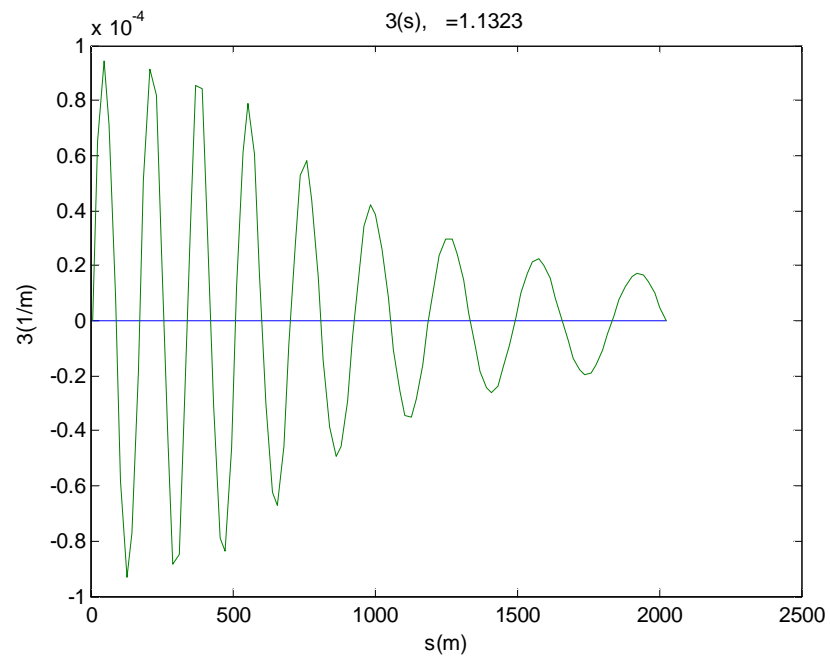
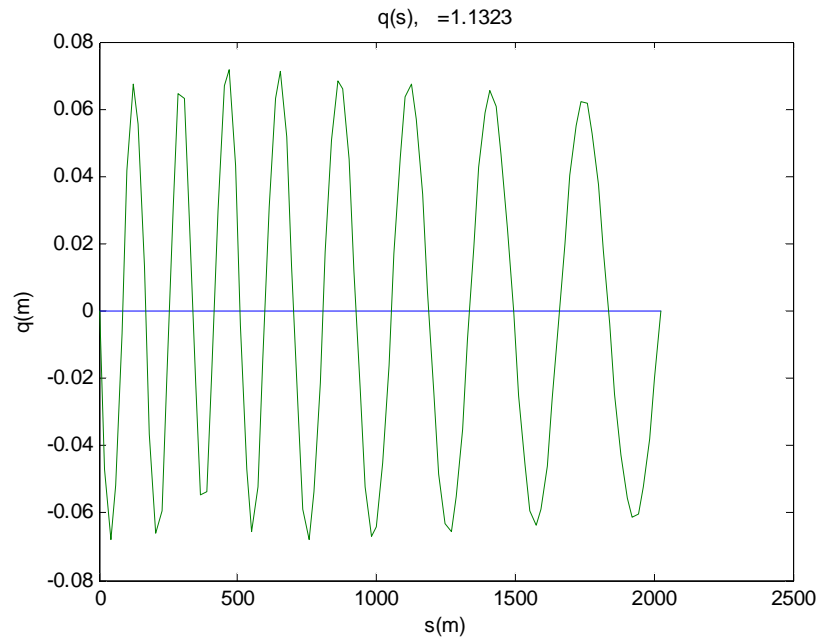
- 6 , =0.8243



- 7 , =1.0534



- 8 , =1.1323



- 9 , =1.2978

